



# European Working Group

## INTERNAL EROSION AND FILTERS :

## UPDATE AND NEW TECHNICAL BULLETINS

MADRID 16 04 10

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P





1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

# Update and new ICOLD bulletins

- Update of bulletin on filters
- Update of bulletin on geotextiles  
and
- A bulletin on risk assessment of  
internal erosion
- A bulletin on methods of detection





# Why an update of the bulletins on granular and geotextile filters?

- A more integrated approach
- A better understanding of material behaviour
- New research results

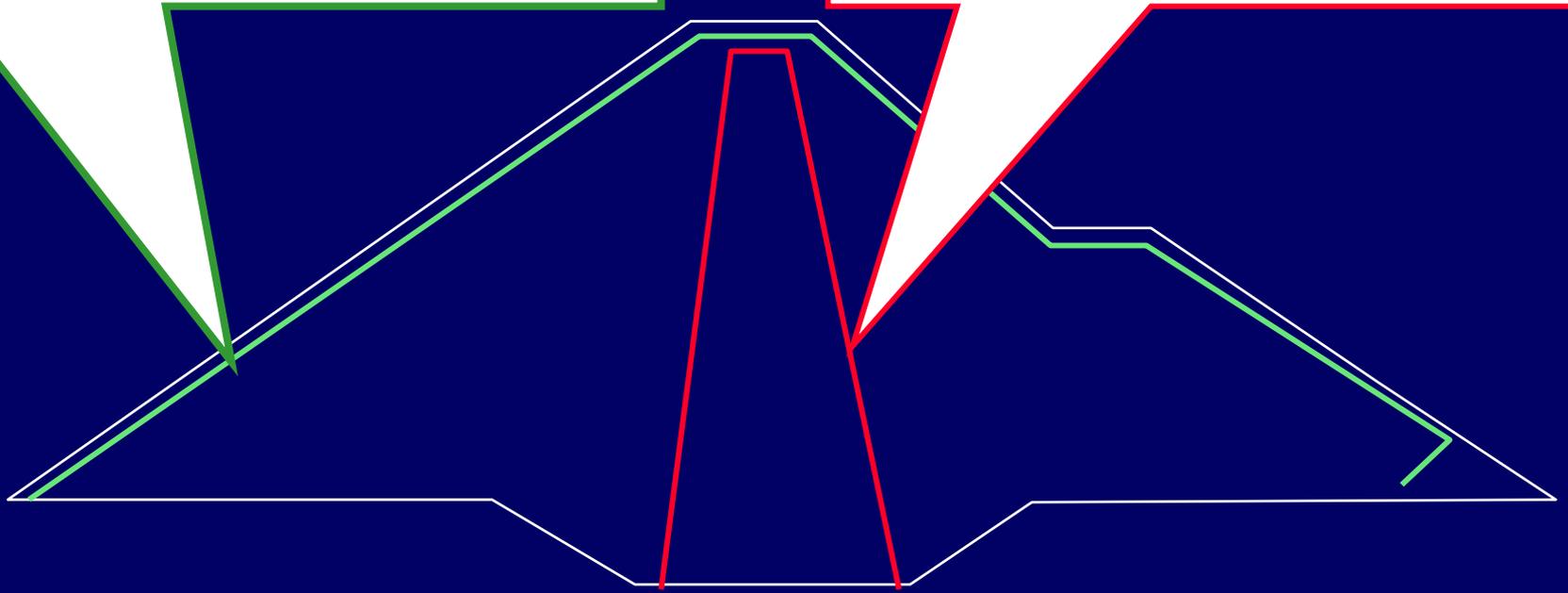


# Two kinds of filter destination

1

- low retention requirement
- High pore pressure requirement

- High retention requirement
- Low pore pressure requirement



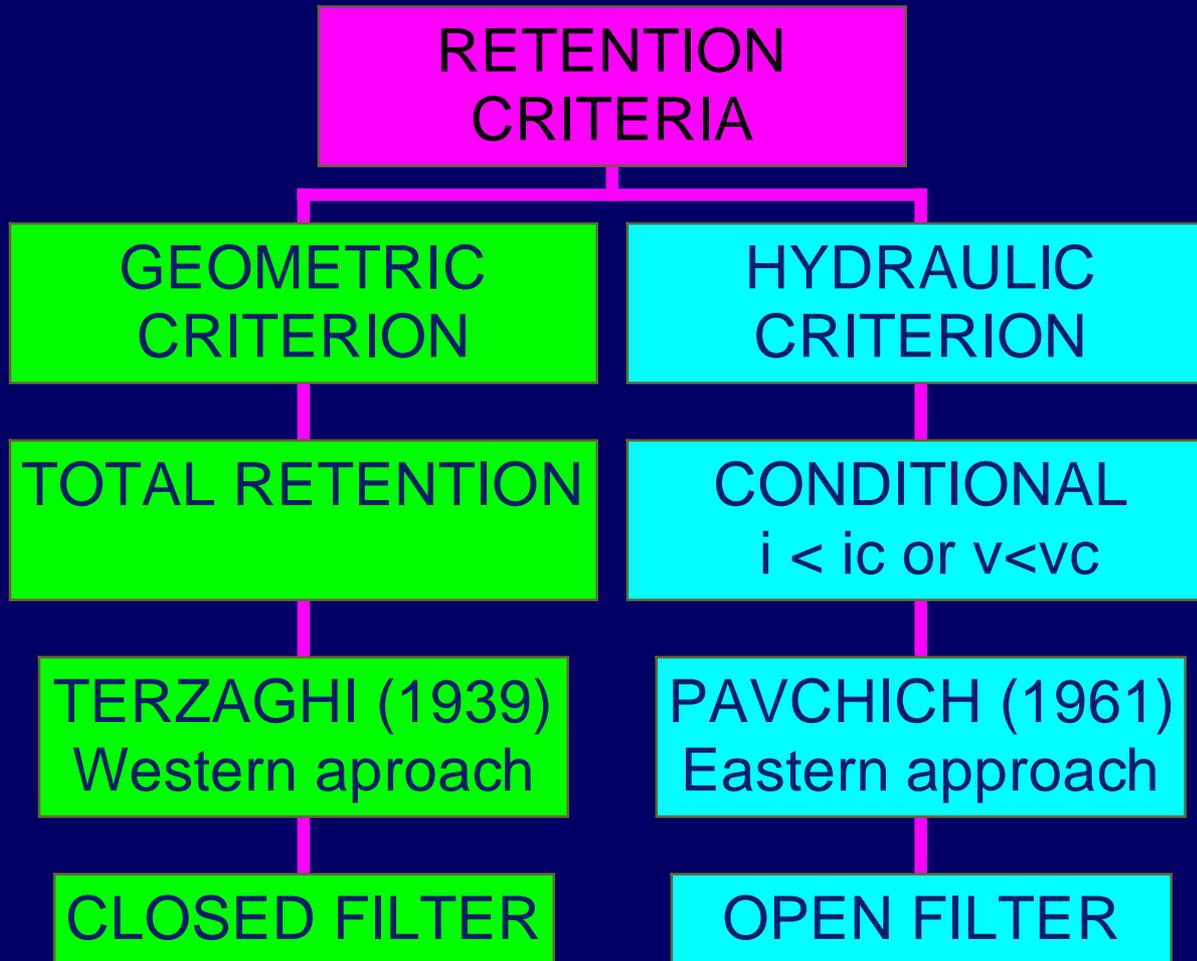
**Critical Filter** : with large concern on dam safety  
**No critical Filter** with low concern on dam safety

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# Two kinds of Retention Criteria



1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

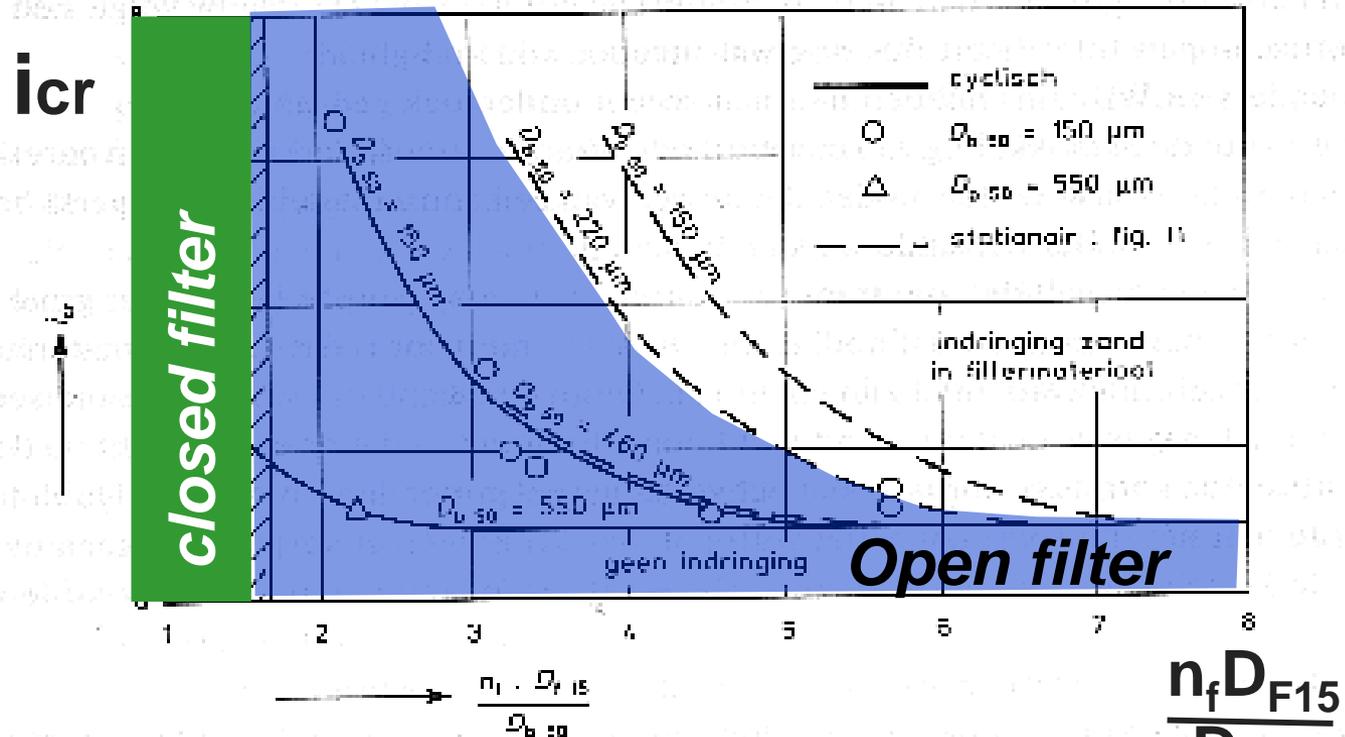




# Open Filters from Bakker K.J. and CUR (1994)

*Open filter : Retention depends on hydraulic gradient*

**Critical hydraulic Gradient Depends on the base soil gradation. Criterion linked to velocity and turbulence**



Flow perpendicular to interface

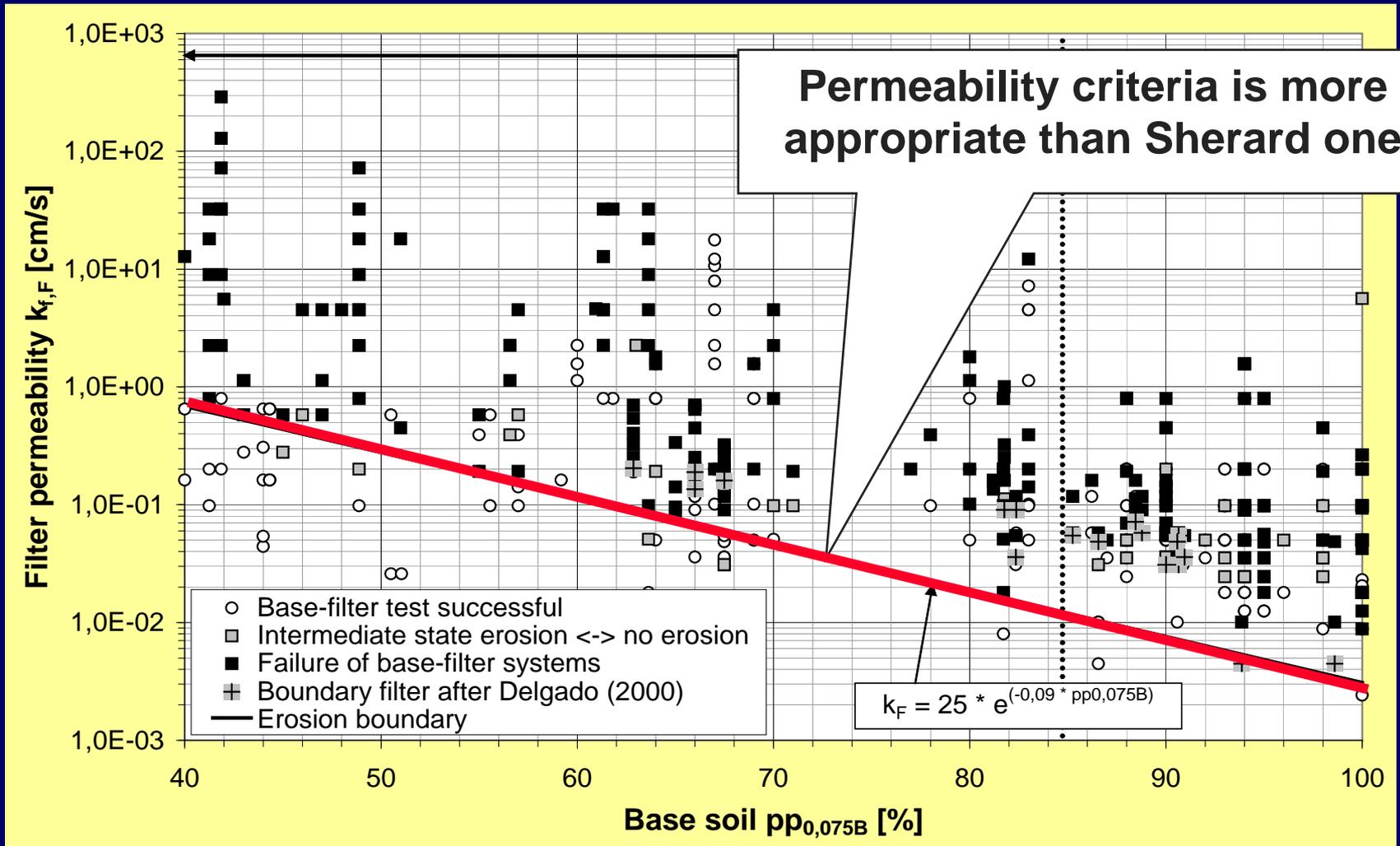
1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P





# New Retention criterion (Delgado)

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P





# Other criteria from Giroud (2010)

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

CRITERIA	FILTER TYPE	CLOSED GRANULAR	OPEN GRANULAR	GEOTEXTILE
RETENTION	POROSITY		X	X
	THICKNESS		X	X
DRAINAGE	PRESSURE		X	X
	FLOW RATE	X	X	X

The advantage of the closed filter is simplicity...





# Geotextile functional characteristics

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

•  $d_{\text{fines}} \leq \text{Filtration Opening Size} \leq d_{\text{skeleton}}$

•  $T_{\text{mini}} \leq \text{Thickness} \leq T_{\text{maxi}}$

•  $K_{\text{mini}} \leq \text{Permeability}$

•  $\text{Porosity / Opening area} \geq n_{\text{mini}}$



# Geotextile functional characteristics

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

•  $d_{\text{fines}} \leq \text{Filtration Opening Size} \leq d_{\text{skeleton}}$

•  ~~$T_{\text{mini}} \leq \text{Thickness} \leq T_{\text{maxi}}$~~   $\longrightarrow 25 \leq m \leq 40$

• **Permeability**  $\geq K_{\text{mini}}$

Homogeneity

Soil  
stability

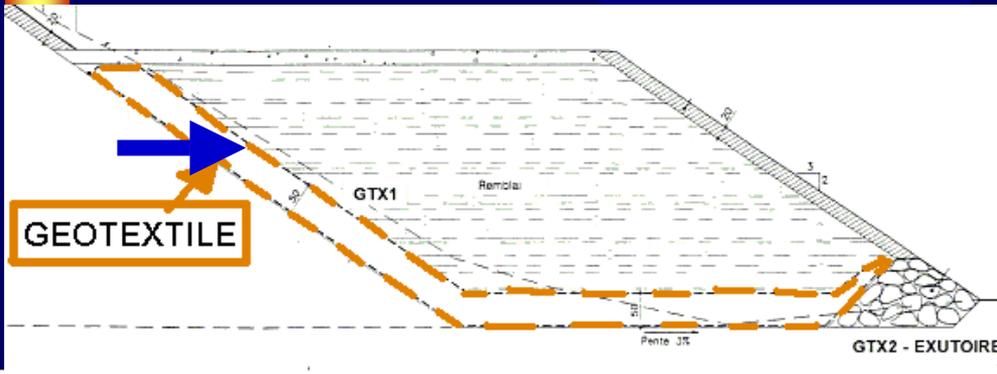


# Some recommendations on limits of the geotextiles use

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I



Torcy dam  
Root hole  
(Royet  
1997)





# Why a new bulletin on internal erosion ? (Foster 1999)

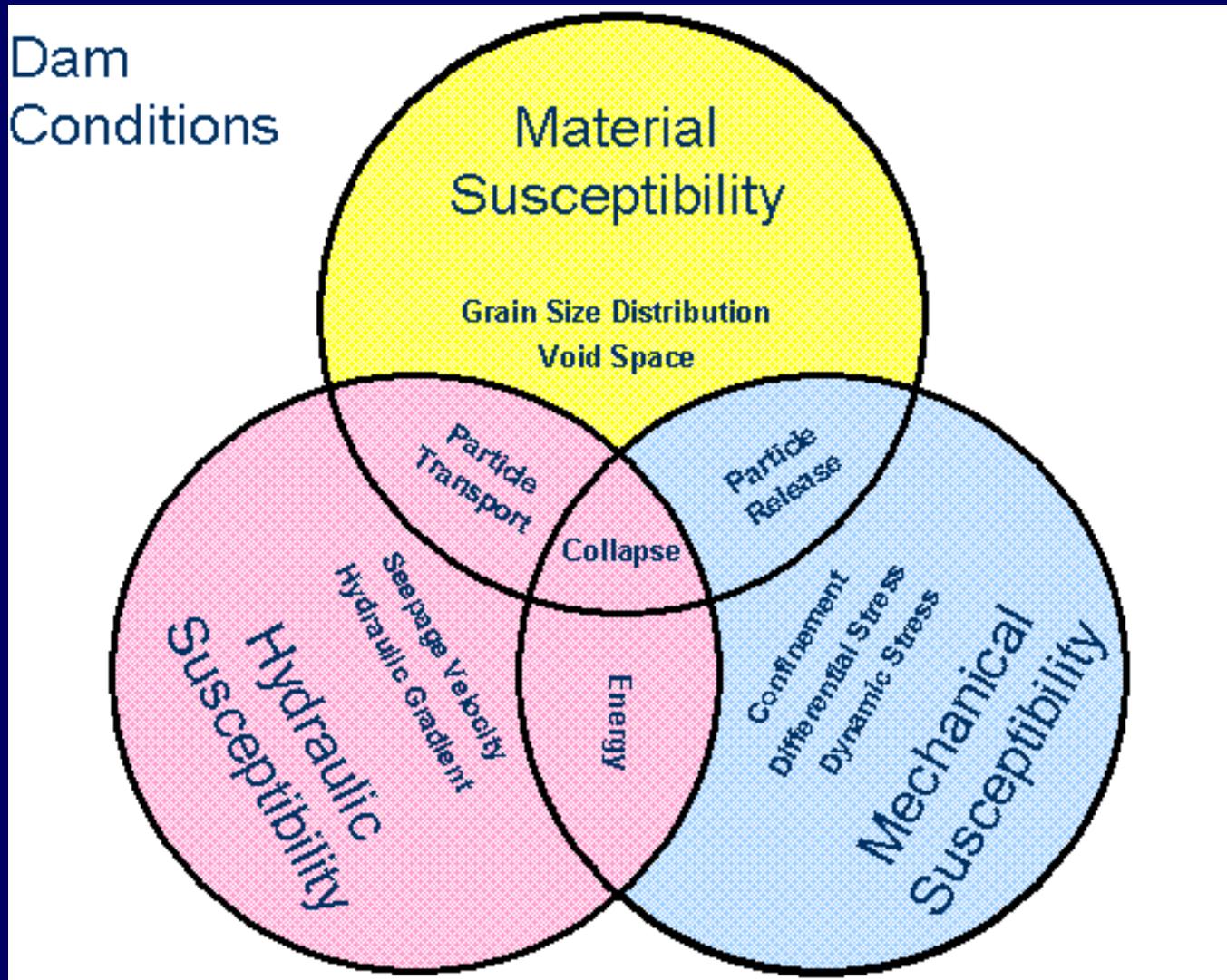
1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

Failure mechanism	Erosion		sliding	
	External Erosion	Internal Erosion	Static shear	Seismic shear
% over the world	48%	46%	6%	
% over the world	94%		6%	





# Rapid screening assessment



1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

The 3 dam conditions (S. Garner 2009)



# How deeply assess the vulnerability?

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

What are the loading conditions ?

Where are the possible locations of initiation?

What are the possible mechanisms of initiating erosion?

What is the filter efficiency in controlling erosion?

What are the consequences of the on going erosion?

Are the consequences detected?

What are the solutions of quick and efficient repair?

What breach mechanism may develop?

What are the consequences & protective measures?



# The framework (Fell & Fry 2007)

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

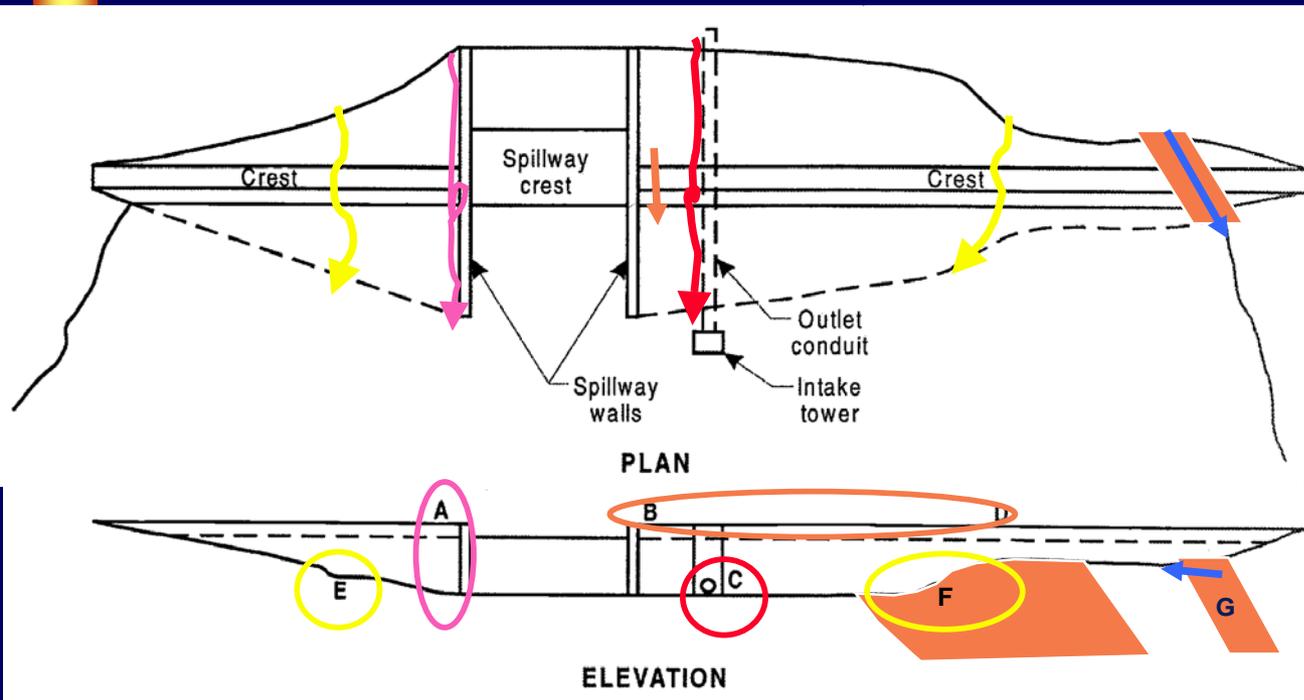
STEPS	QUESTIONS AND ANSWERS
<b>1 Loading</b>	HYDROSTATIC : Frequent water level, Rare flood, Safety flood SEISMIC : OBE and MDE
<b>2 Location</b>	EMBANKMENT : Upper, Lower, Conduit, Wall, FOUNDATION : Valley, Abutment, EMBANKMENT TO FOUNDATION
<b>3 Initiation</b>	BACKWARD EROSION, CONCENTRATED LEAK, CONTACT EROSION, SUFFUSION
<b>4 Filtration</b>	NO EROSION VAUGHAN, NO EROSION SHERARD, SOME EROSION, EXCESSIVE EROSION, CONTINUING EROSION
<b>5 Progression</b>	Rate of erosion? Will pipe stay open? Upstream and downstream flow limitation? Critical gradient or velocity reaches? Hold a roof?
<b>6 Detection</b>	Piping mode monitoring? Surveillance frequency? Continuous temperature measurement?
<b>7 Intervention</b>	Safety measures for piping mode? Personnel? Equipment? Materials? Weather? Flooding? Access? Training? Time to intervene?
<b>8 Breach</b>	GROSS ENLARGEMENT, LOSS OF FREEBOARD by CREST SETTLEMENT, SLOPE INSTABILITY, UNRAVELLING





1  
6  
0  
4  
2

# Location of initiation : Where are the Failure paths?



## LEGEND

- A, B Adjacent spillway walls.
- C Adjacent outlet conduit.
- D,E Related to irregularities in the foundation profile.
- F In the foundation
- G From embankment to foundation





# Factors of initiation

## Poor Design

- No filter (old dams)
- Bad filters
- Embankment zoning
- High permeability zone

## AGEING

- Conduit leak
- Structure ageing
- Filter degradation
- Incomplete repair
- Differential settlement of the foundation
- Dessication cracking
- Animal holes
- Vegetation

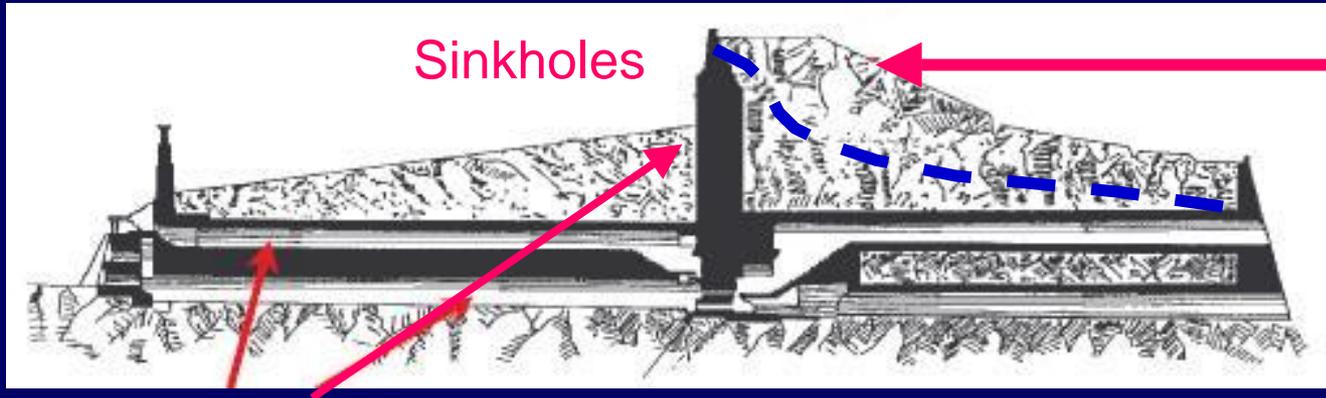




# St-Ferreol ageing (1675)



1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P



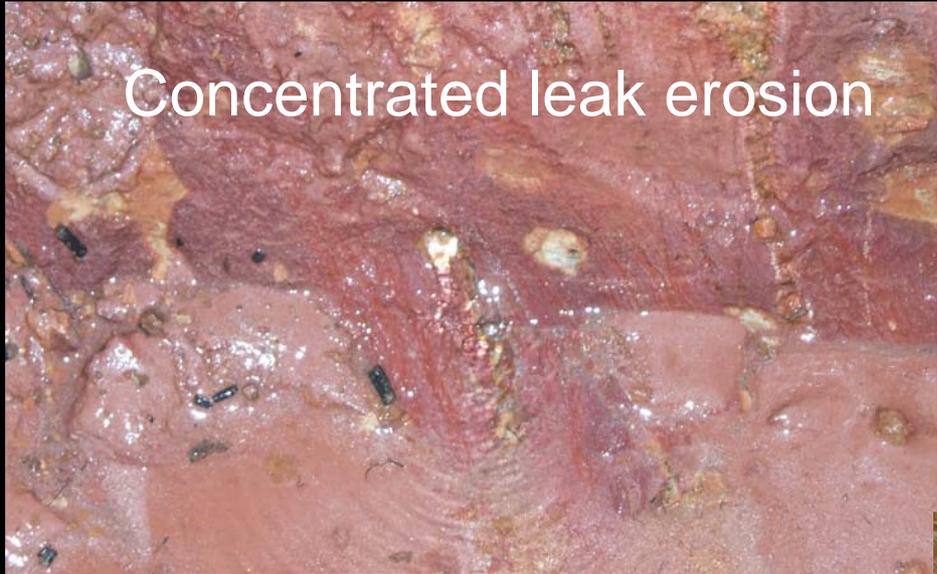
Leakage 6l/s, sinkholes and sand and gravel deposit in the conduit (some m<sup>3</sup>)





# Filter weathering and clogging

Concentrated leak erosion



Large leakage with clay deposit in collector



Filter weathering and clogging





# Initiation : definition

**Internal erosion** occurs when soil particles within a water retaining structure or its foundation, are carried downstream by seepage flow. Internal erosion can initiate by 4 types of initiation :

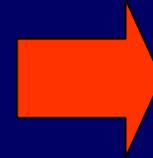
- 1 Concentrated Leak Erosion,
- 2 Backward Erosion,
- 3 Soils Contact Erosion,
- 4 Suffusion.





# 1 – crack or hole erosion

## Clayey fill on clay foundation



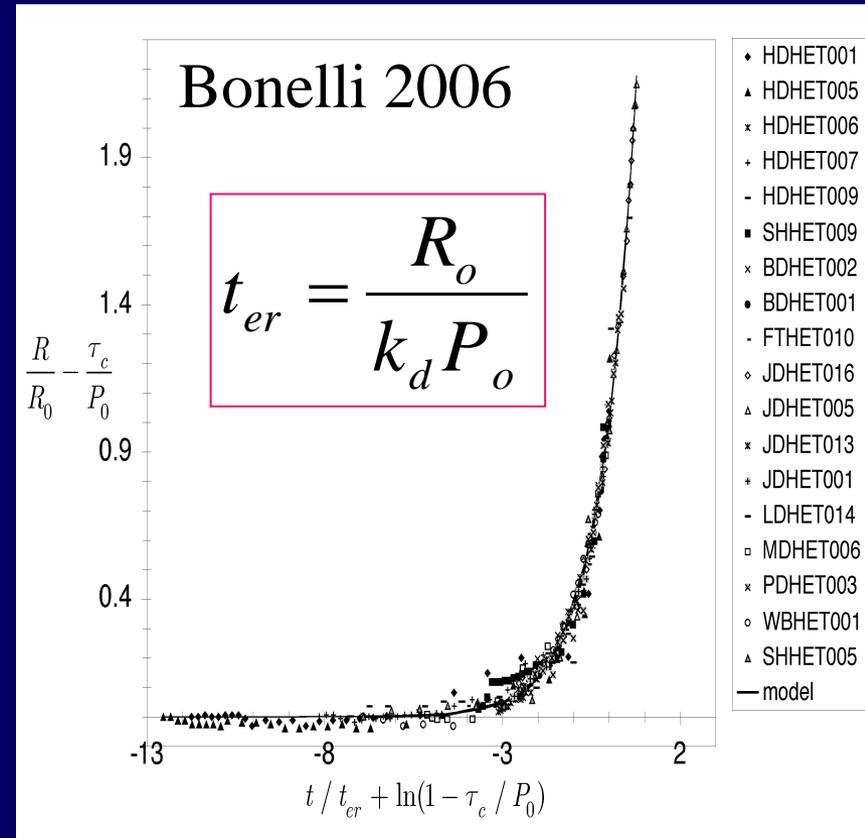
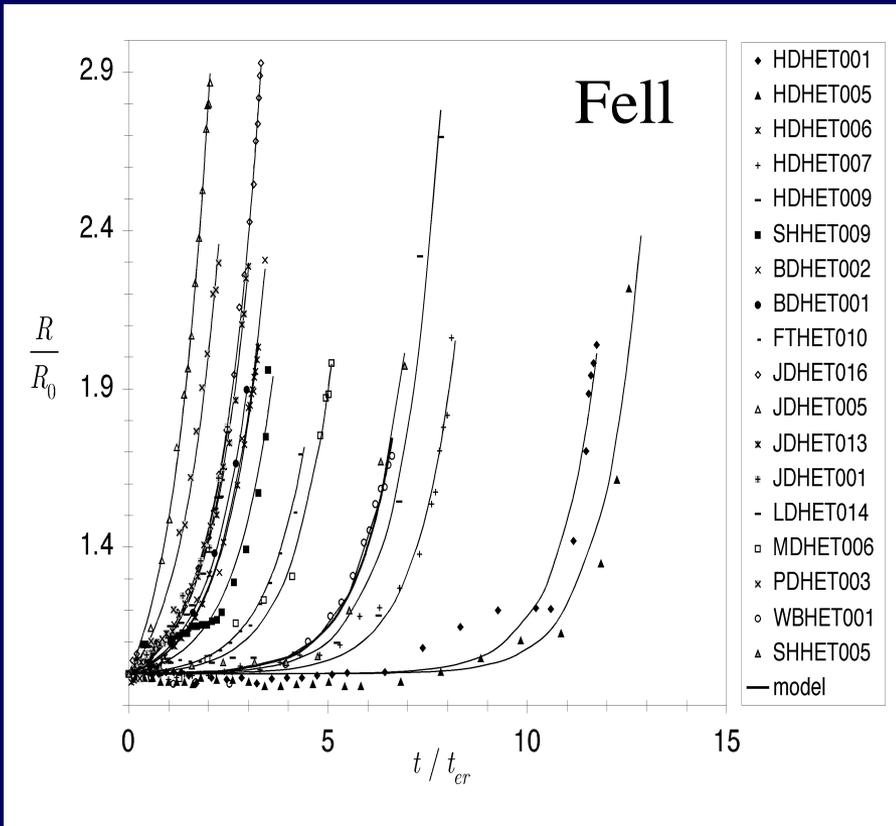
Test de HET  
(CEMAGREF  
LCPC)





# 1 – crack or hole erosion

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P



Only one relationship, but different time scales!





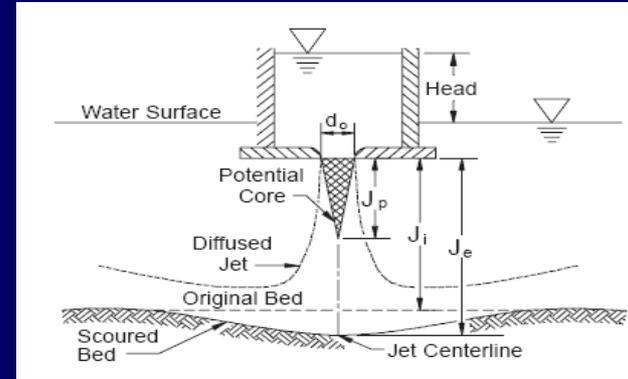
# 1 – crack or hole erosion

sandy clay or silt material



whether HET  
impossible

=> JET test



=>  $kd, \tau_c$

Dispersion  
(castle test)



M  
A  
D  
F  
I  
D  
C  
N  
E  
C  
P



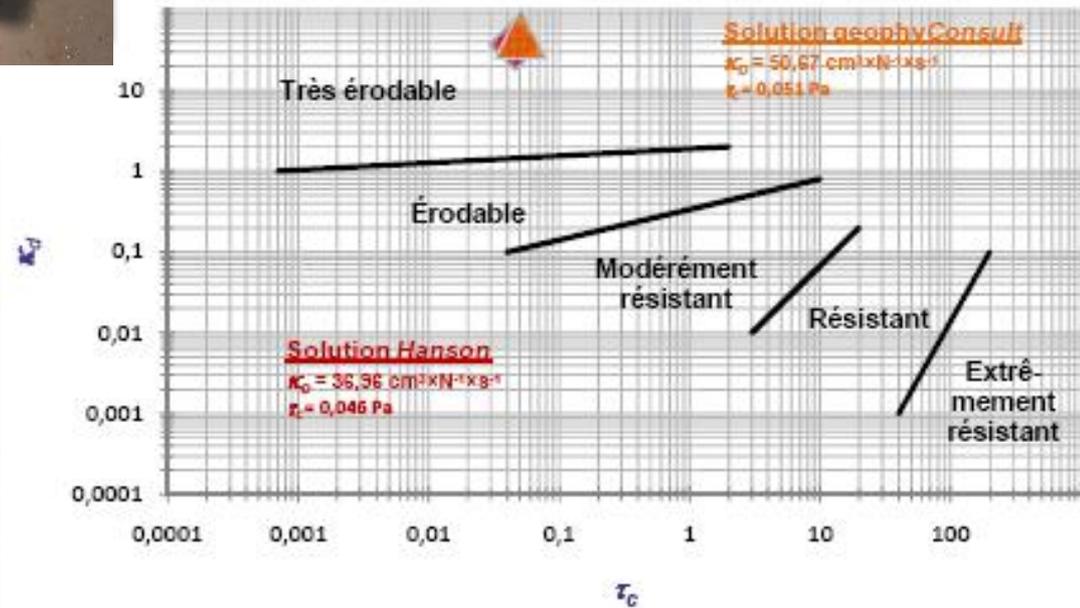


# Erosion test used as an Index test

JET test result on residual soil :

= Very large erodibility

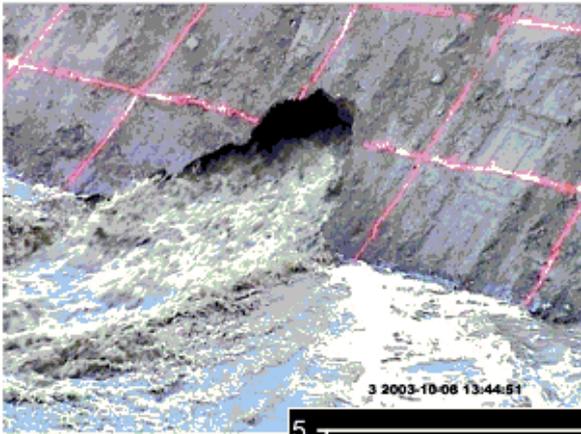
=> **very urgent repair**





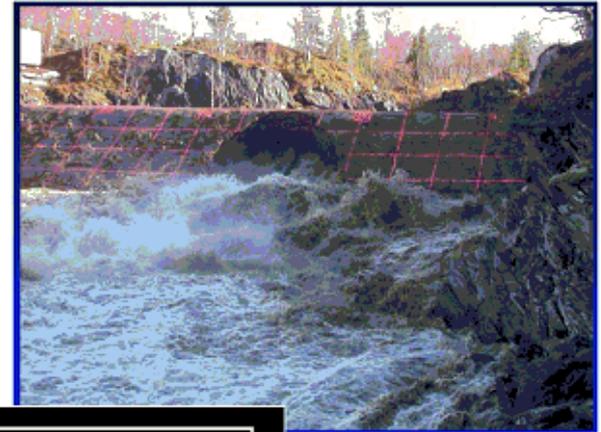
# 1 – crack or hole erosion : application of tests to piping

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

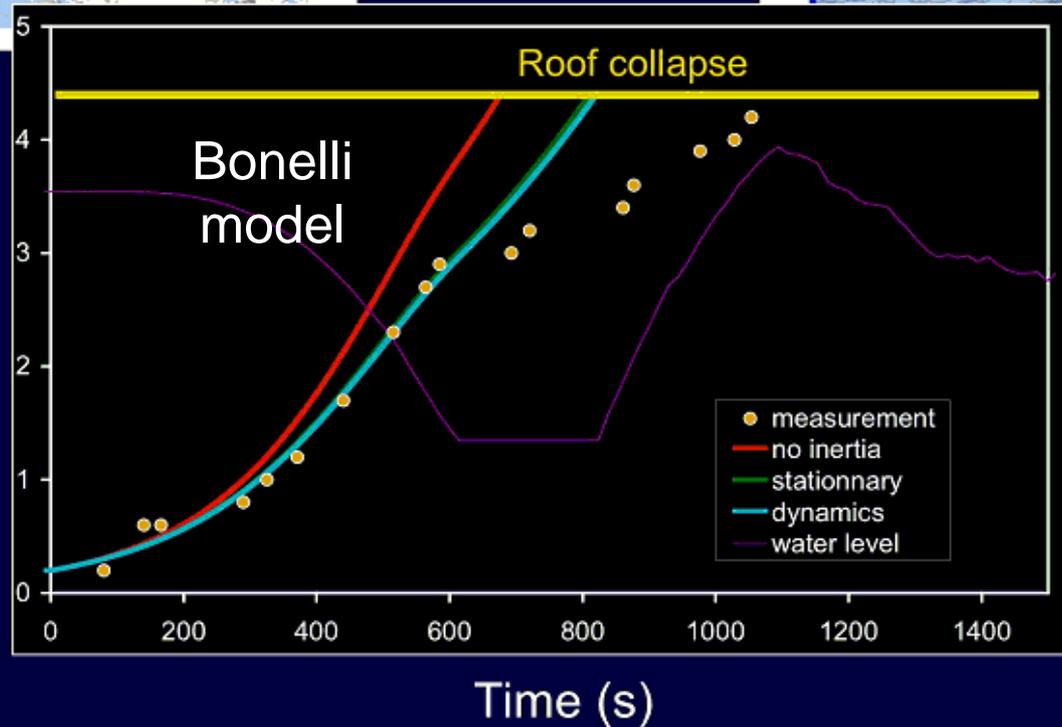


Norway  
*IMPACT*  
FP5 Project

Rossvatn  
field tests



Radius (m)



$$\tau_c \approx 5 \text{ Pa}$$
$$k_{er} \approx 10^{-2} \text{ s/m}$$

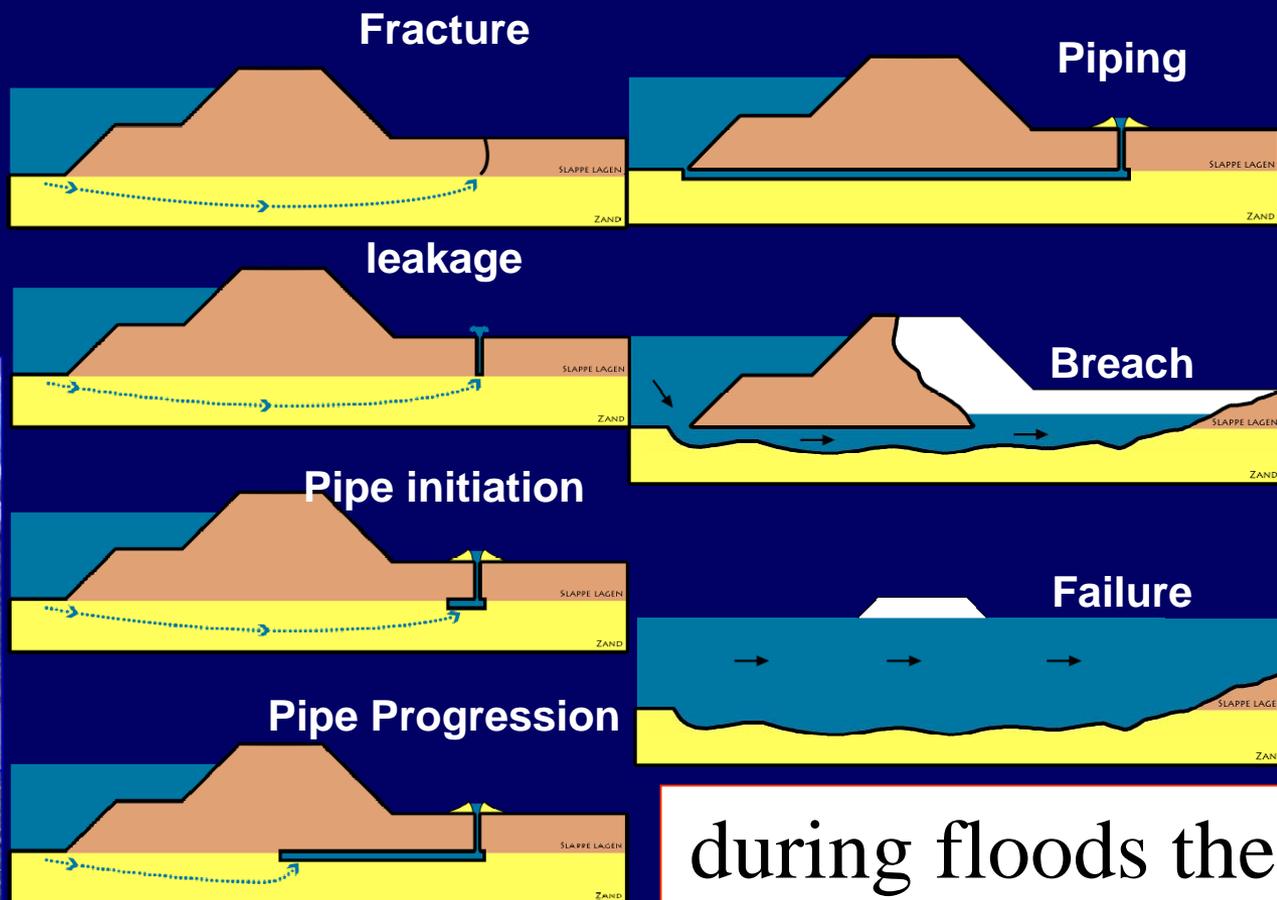




# 2 - Backward erosion

## Clayey embankment on sandy foundation

1



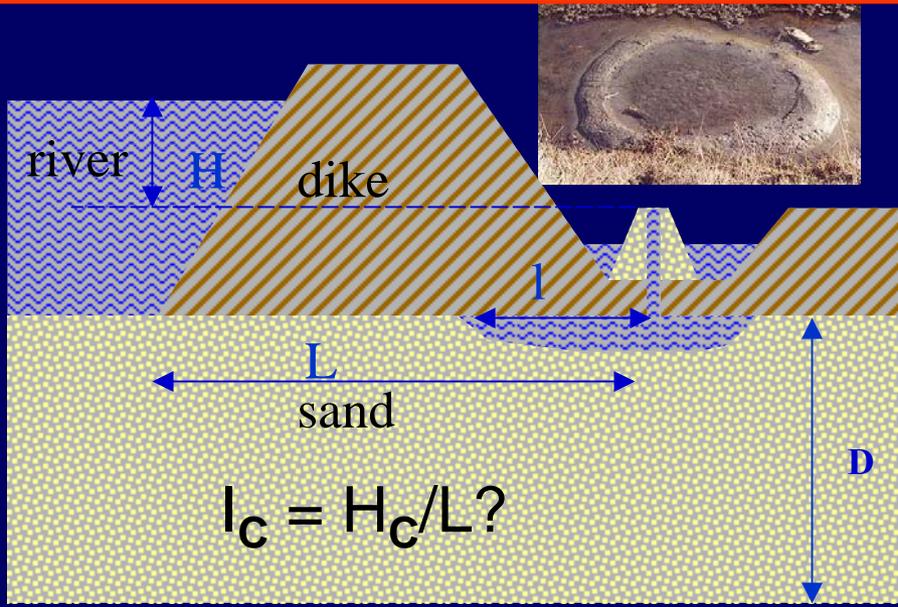
during floods the  
pipe increases  
up to failure





# 2 - Backward erosion

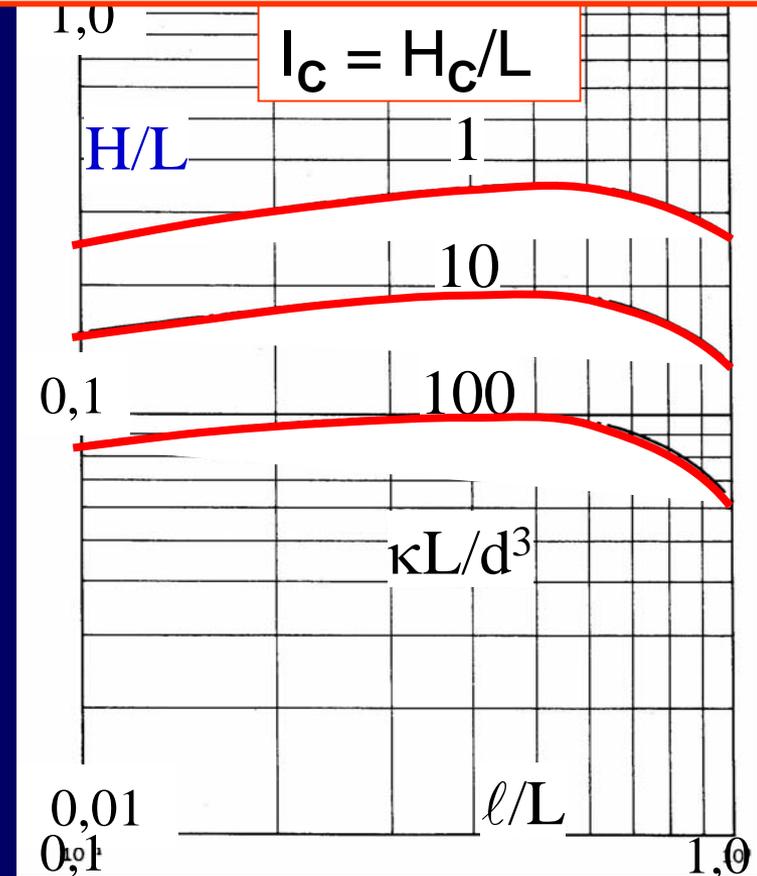
## Clayey embankment on sandy foundation



$$\Delta H_c = \alpha \cdot c \cdot \frac{\gamma_p}{\gamma_w} \tan(\theta) (0.68 - 0.10 \ln(c)) \cdot L$$

$$\alpha = \left( \frac{D}{L} \right)^{\left( \frac{0.28}{\left( \left( \frac{D}{L} \right)^{2.8} - 1 \right)} \right)}$$

$$c = \eta d_{70} \left( \frac{1}{\kappa L} \right)^{\frac{1}{3}}$$



Sellmeijer (1988)

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# 2 - Backward erosion in karstic foundation

1  
6



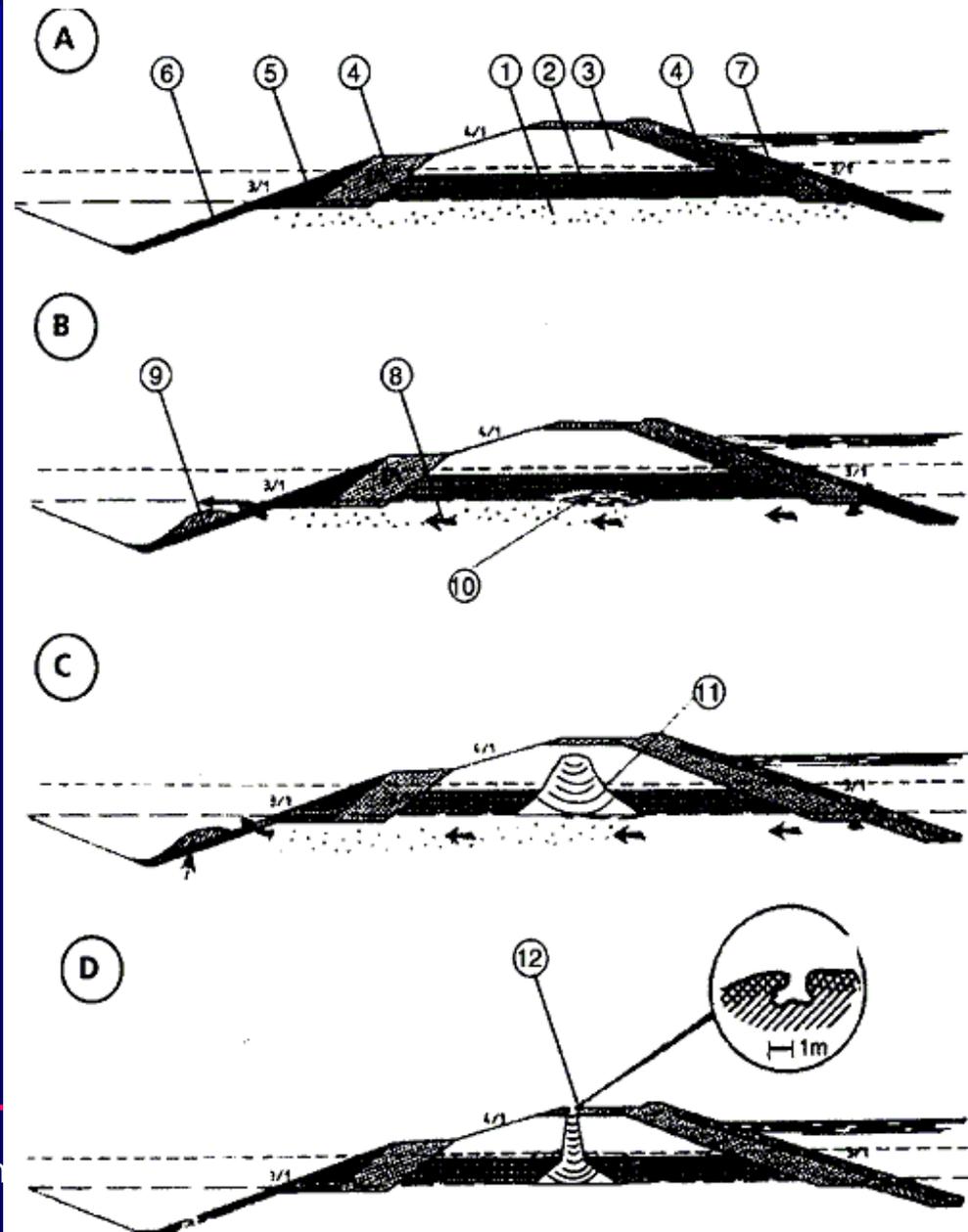
El Gassanieh reservoir (2003)  
during an extreme flood

1m water load caused  
the collapse of 3  
sinkholes (15-25 m  
diameter) along a  
fault in the reservoir



# Embankment on gravely alluvium

## 3 Contact erosion



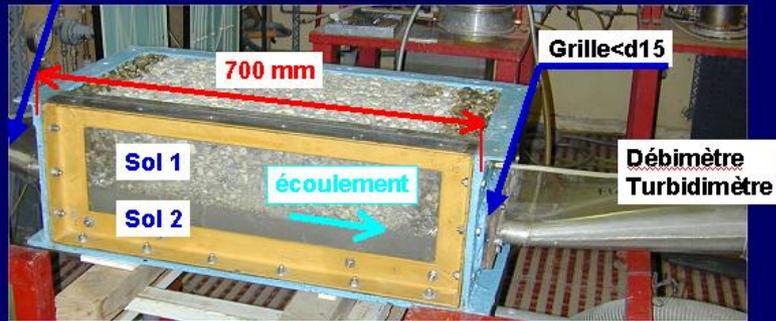
04  
2010  
MADRID  
CNEGP

# Embankment on gravely alluvium

1  
6  
0  
4

## 3 – Contact erosion

Alimentation par un réservoir à niveau constant avec mesure du débit



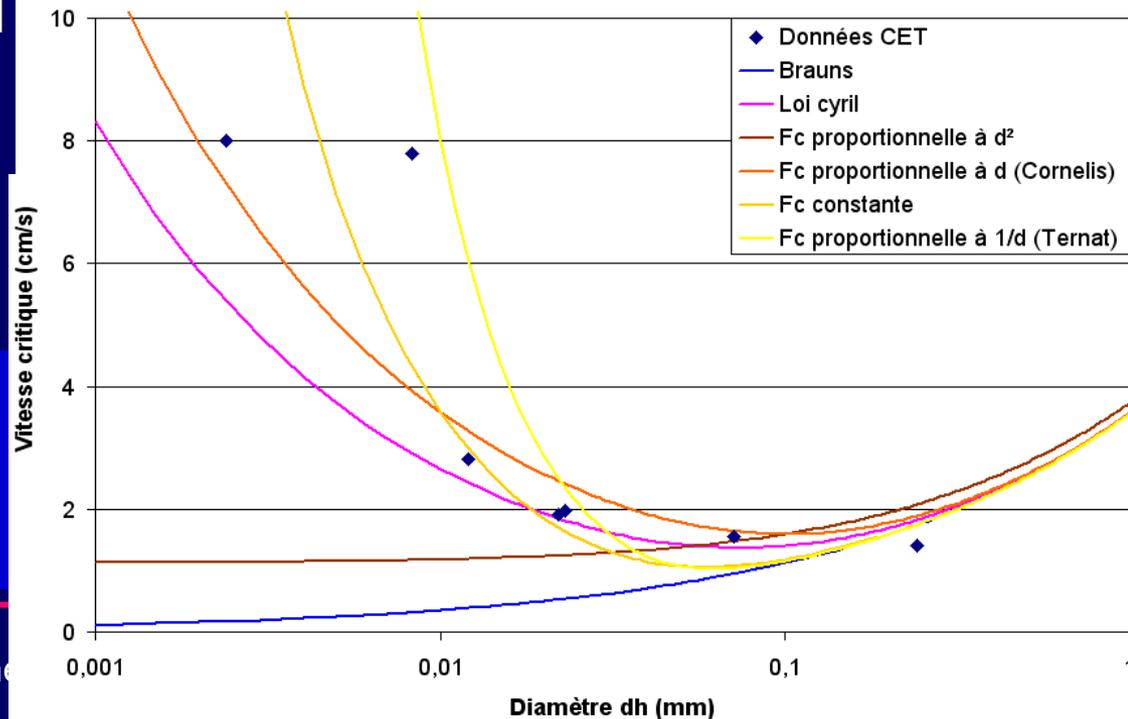
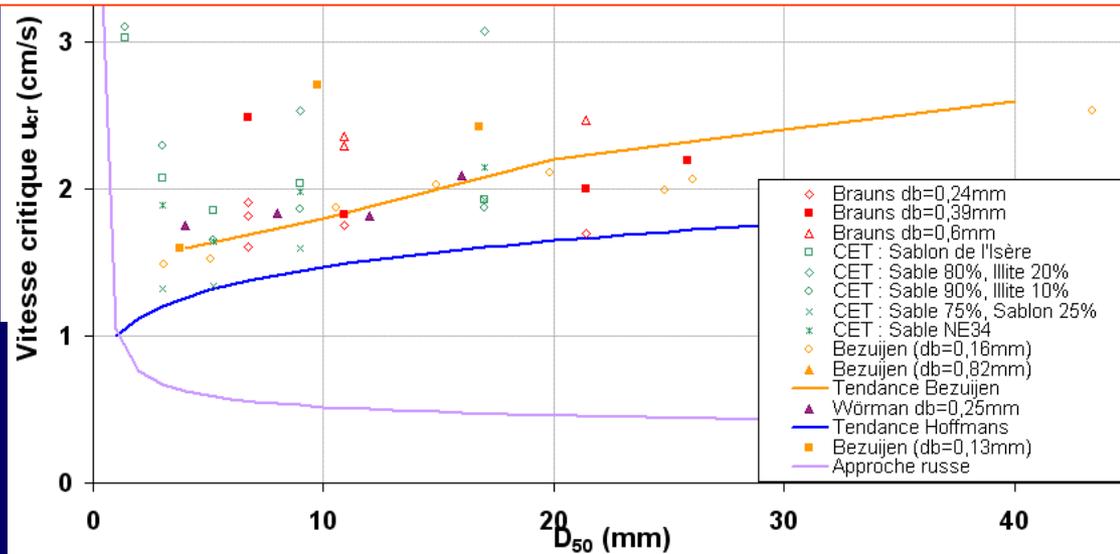
I  
D  
C  
N  
E  
G  
P

LTHE Y-H Faure, C. Guidoux, R. Beguin

No erosion with  $v < \#1\text{cm/s}$

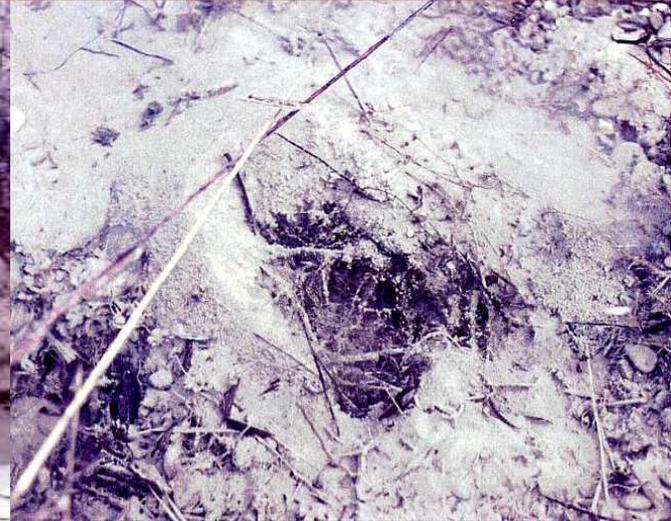


2010 Grenada EWG of ICOLD boletine



# Embankment or foundation with unstable soil

1  
6  
0  
4  
2  
0



4 - Suffusion



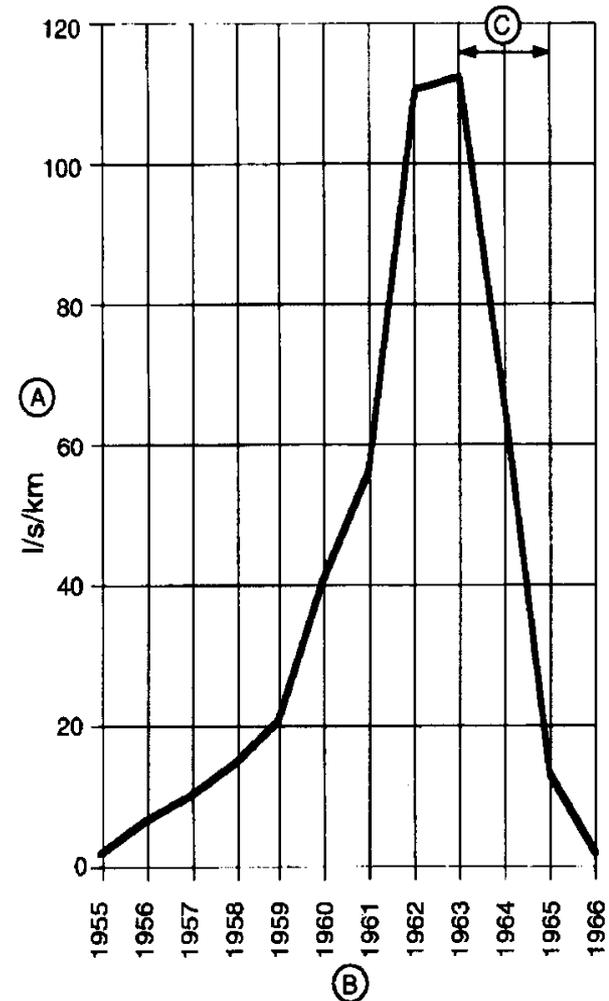
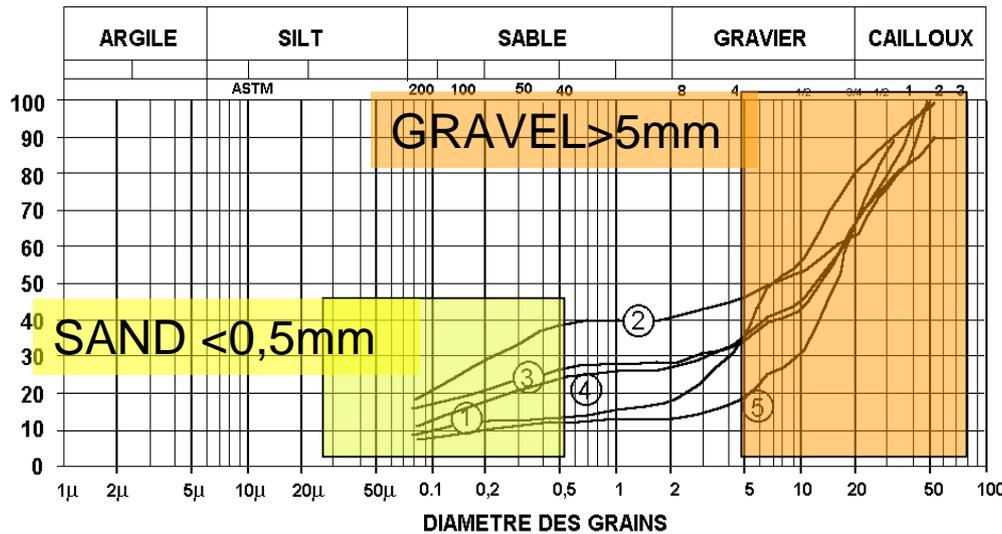
# Embankment or foundation with unstable soil

## 4 - Suffusion

No erosion with

$$V < \# 0,5 \text{ cm/s ?}$$

(M. GOLTZ 2009)



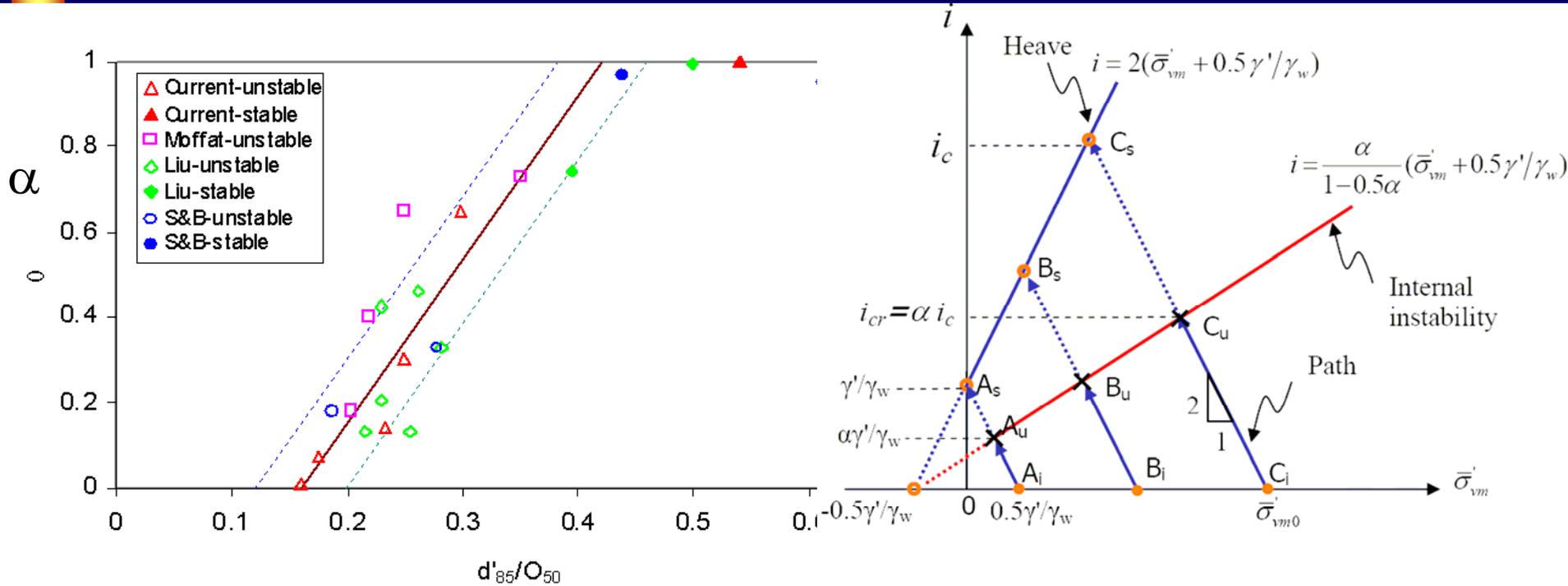
Digue de Cusset - Évolution des fuites au Pk 14.6  
Cusset bank - Point 14.6 leakage variation

- m (A) Specific leakage (l/s/km)
- (B) Date
- (C) Grouting

# Embankment or foundation with unstable soil

1  
6

## Initiation de la suffusion



E  
G  
P

## Geometric et hydromecanic criteria from Fannin (2008)

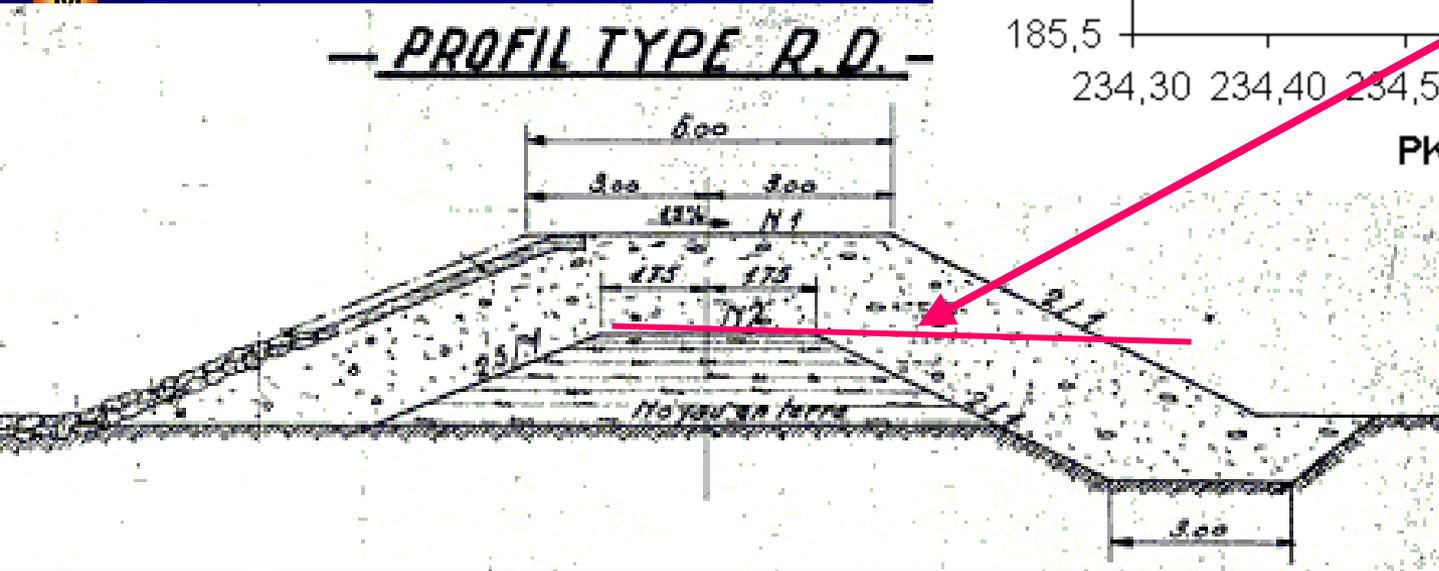
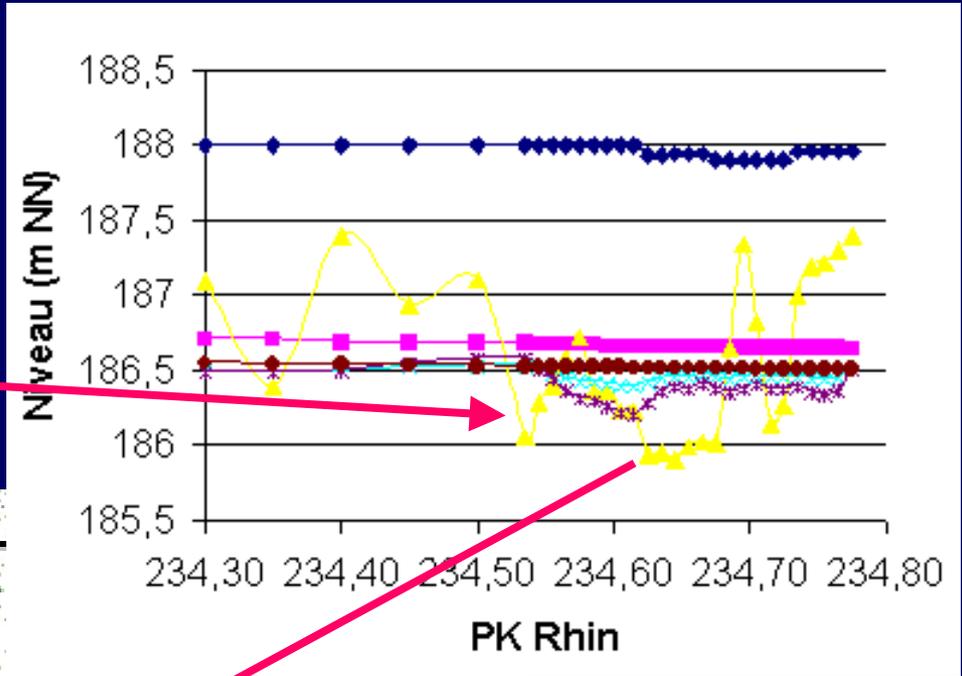


# Contact erosion on Rhine river dike

1  
6  
0  
4  
2  
0  
1  
0  
M

Crest elevation after maintenance

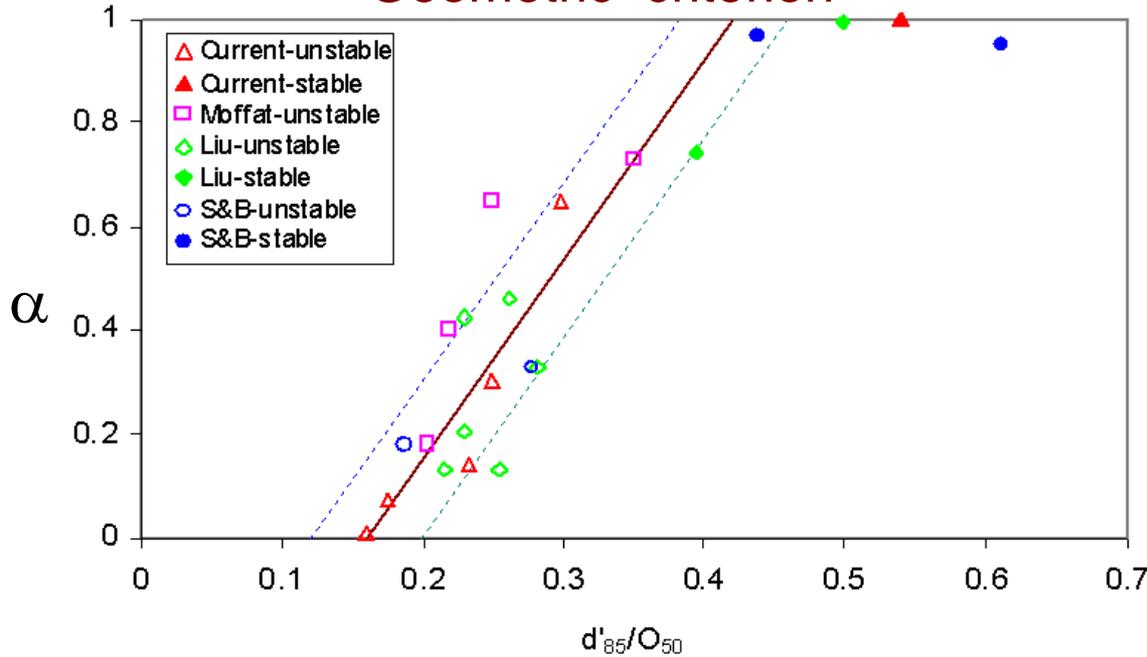
Core elevation



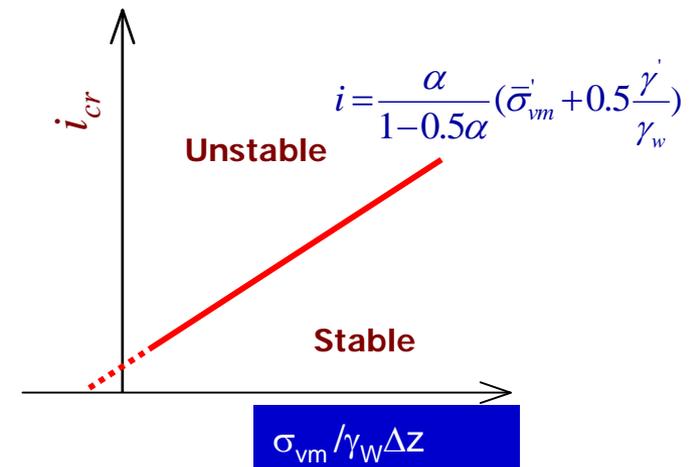


# Initiation of suffusion

### Geometric criterion



### Hydromechanical criterion



## Double criteria proposed by Fannin (2008)





# Why a bulletin on detection methods?

- Too much on internal erosion in one bulletin only
- A lot of possible methods
- New effective methods

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P





# Detection :

the most effective methods

The 3 Safety assessment conclusions :

1 Repair    2 No problem    3 Some Doubts

Remedial  
maintenance :

- SP
- Temperature
- Drill hole recording

Preventive  
maintenance :

- Fiber optic





# Detection by SP in soft foundation

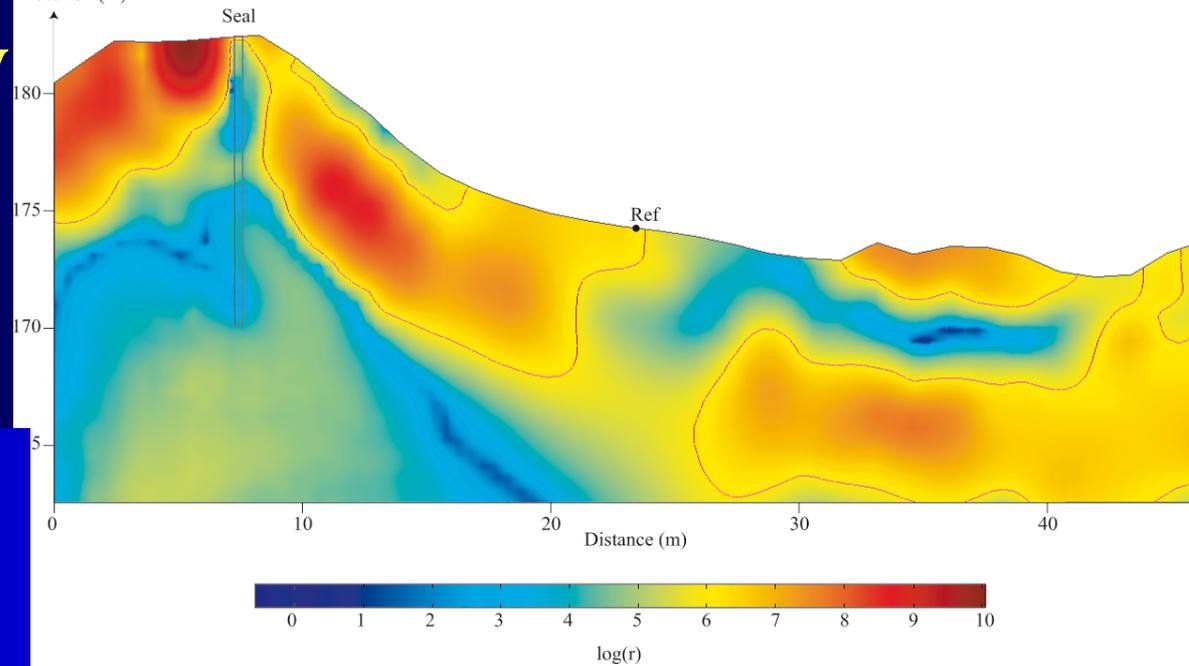
Resistivity

Tomography

(Revil & Bolève 2008)

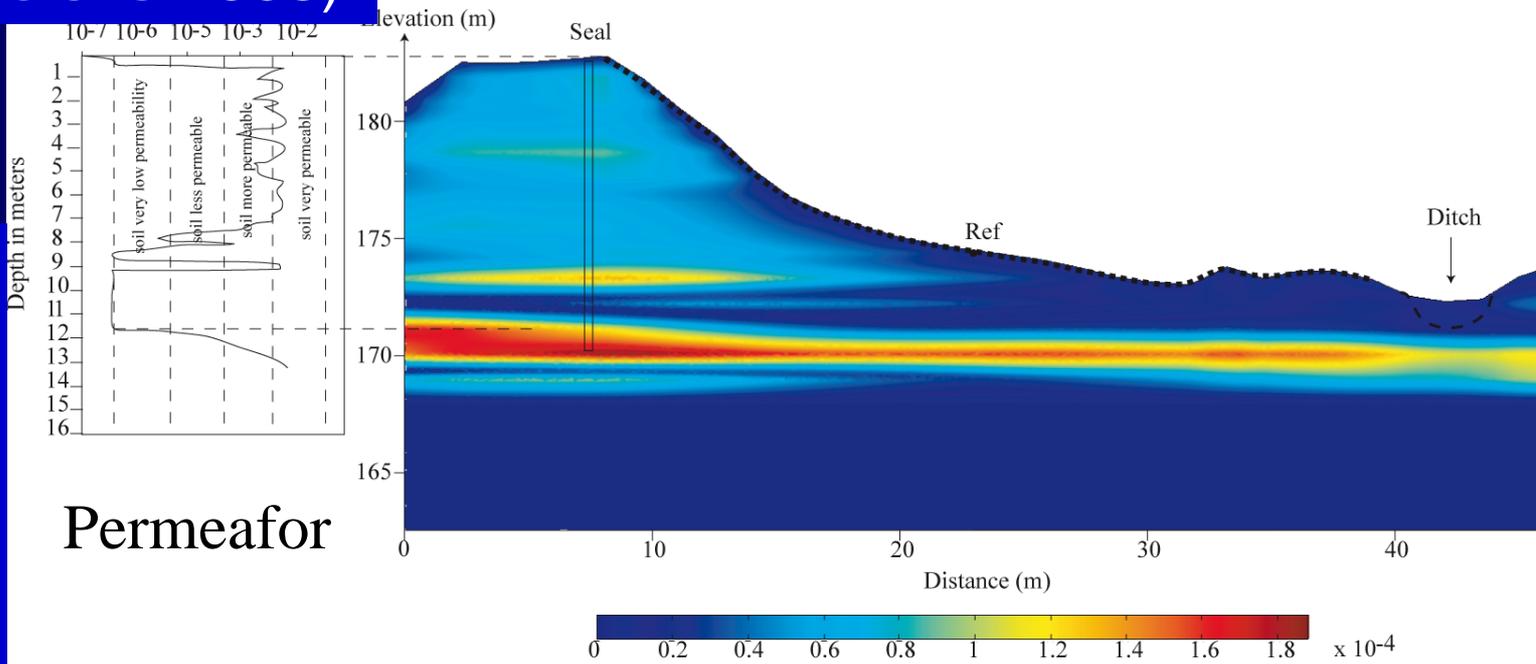
16042010MADRIDCNEGP

Water leaks from External current density



A

B

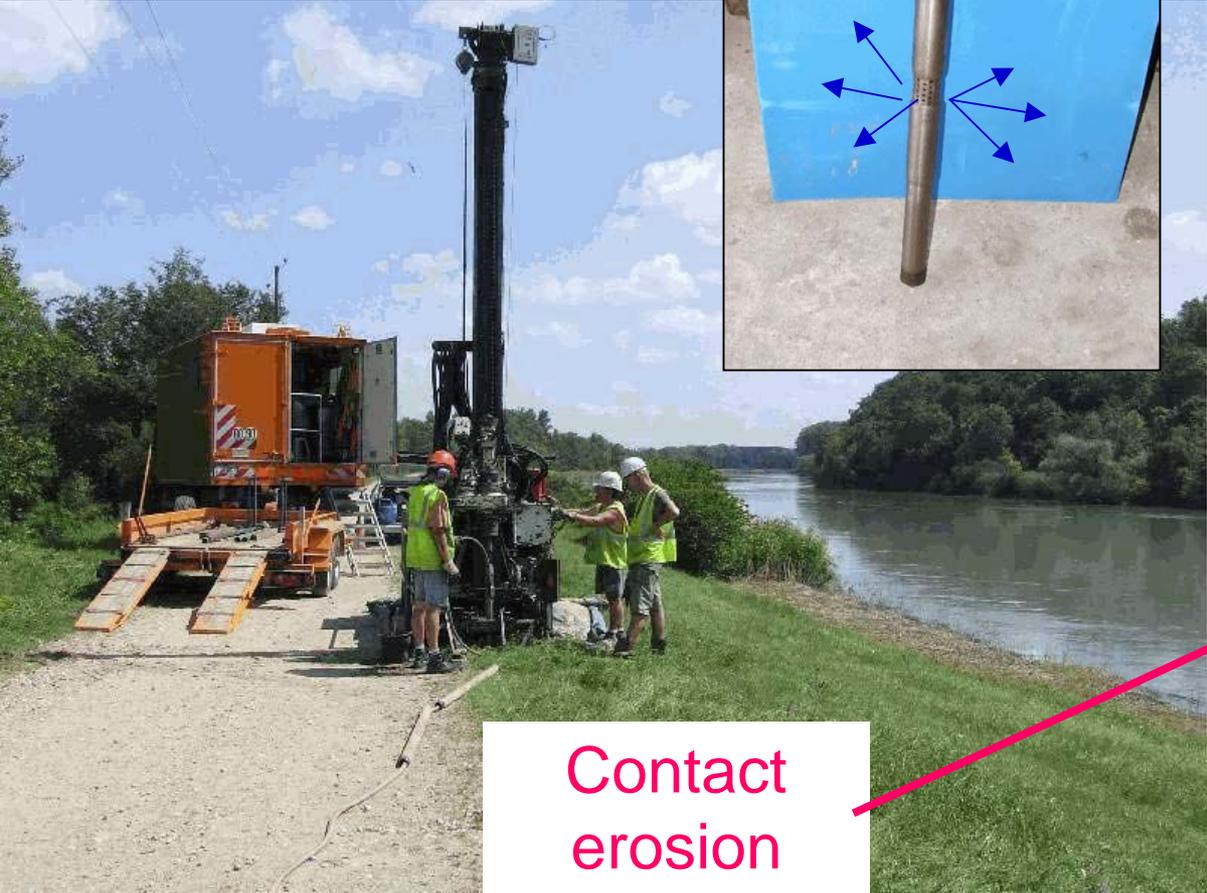


Permeability

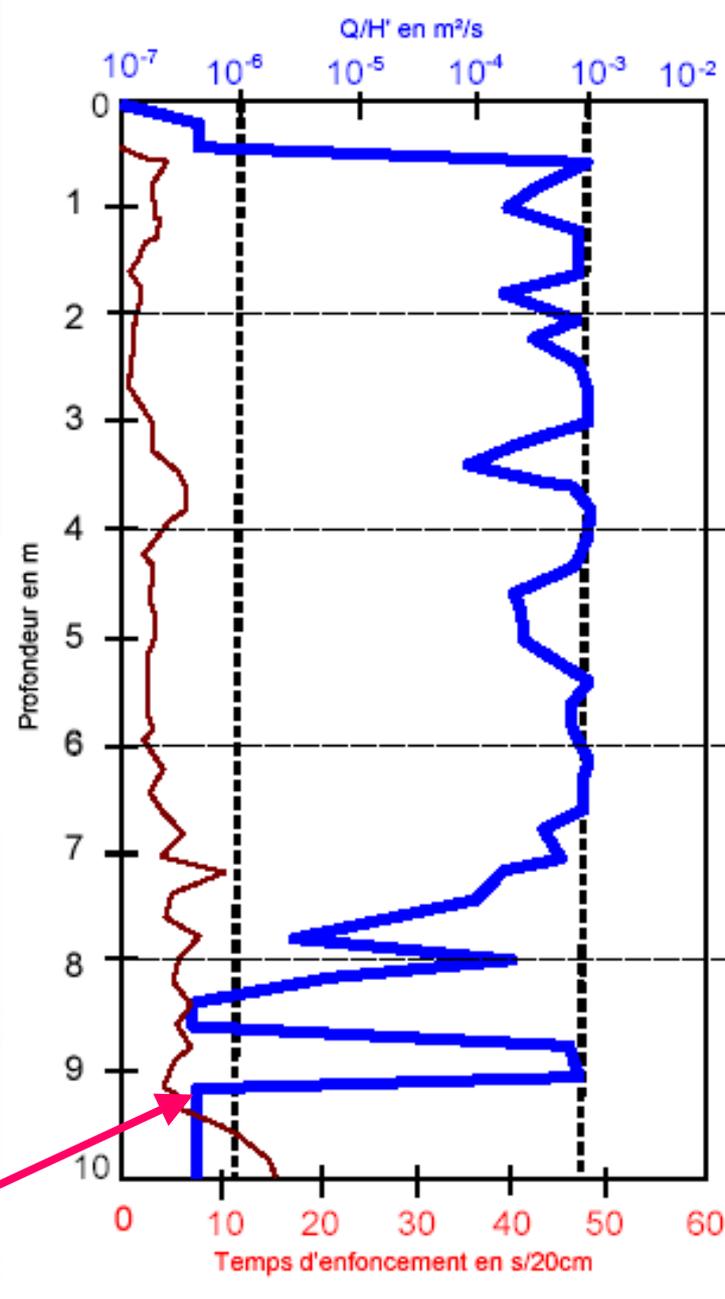


# Detection of contact erosion with Permeafor

1  
6  
0  
4  
2

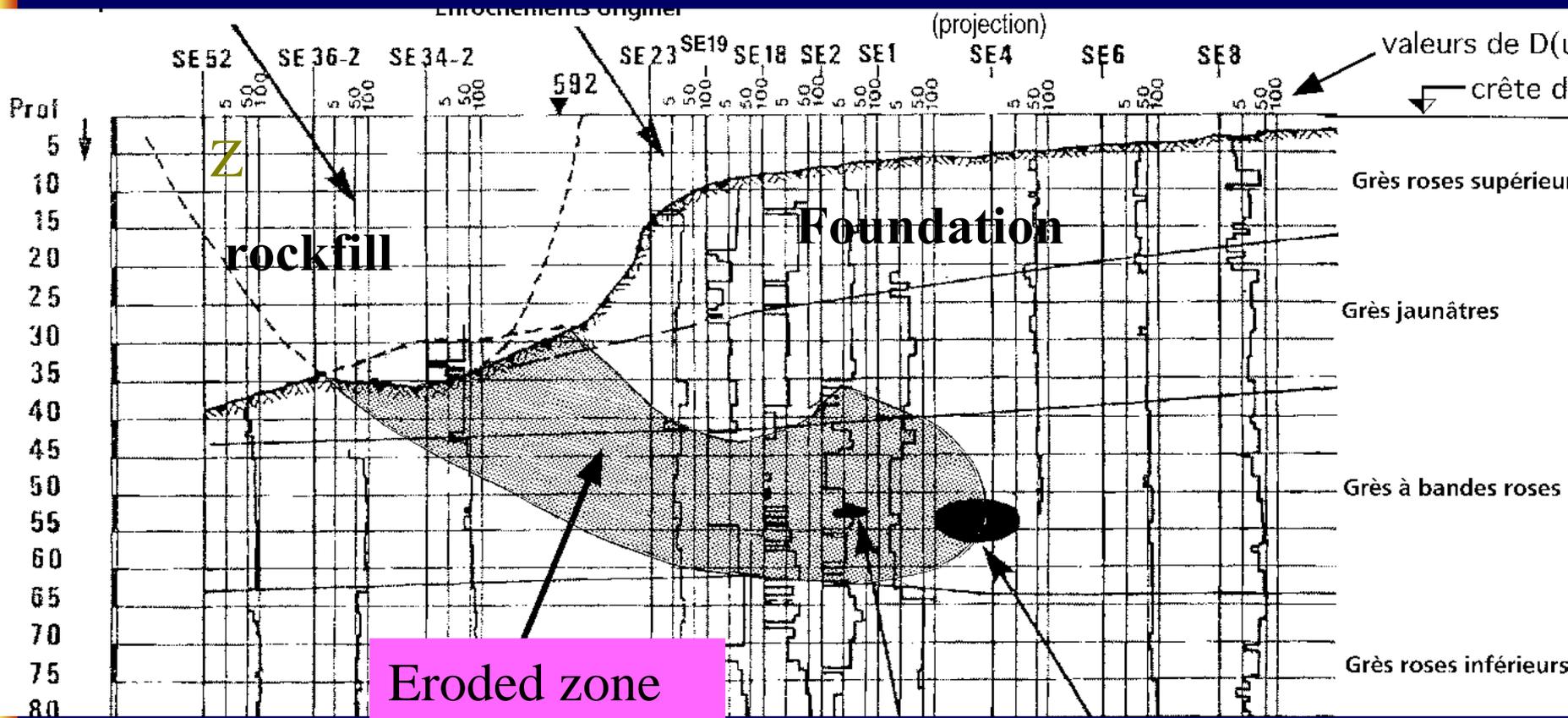


Contact erosion





# Detection at ITIYURO dam



Drilling parameter recording on weak sandstones which suffered internal erosion show very low hardness values :  $DUR < 20$ .

C  
N  
E  
G  
P



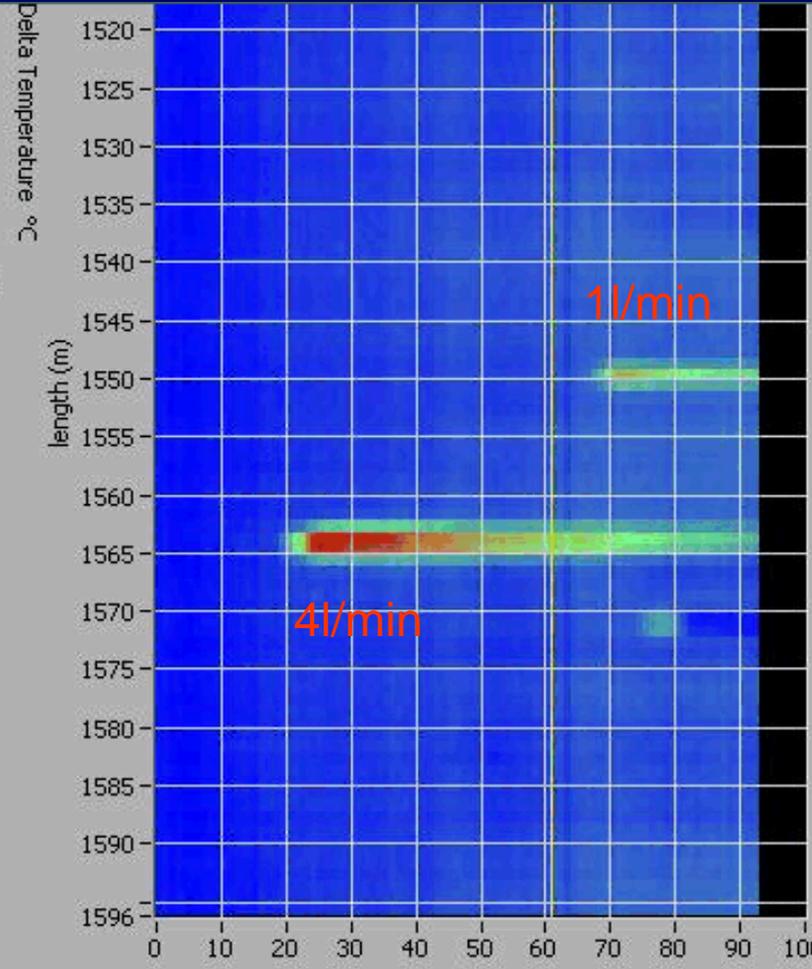


# Preventive maintenance

1  
6

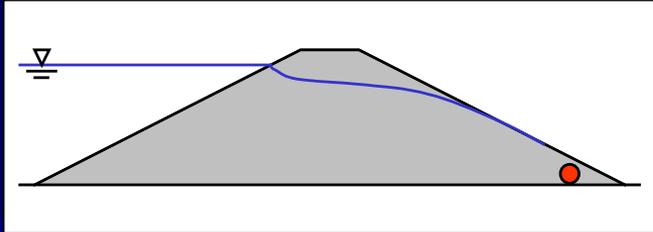
## Oraison canal 2005

## Optic Fiber : passive method

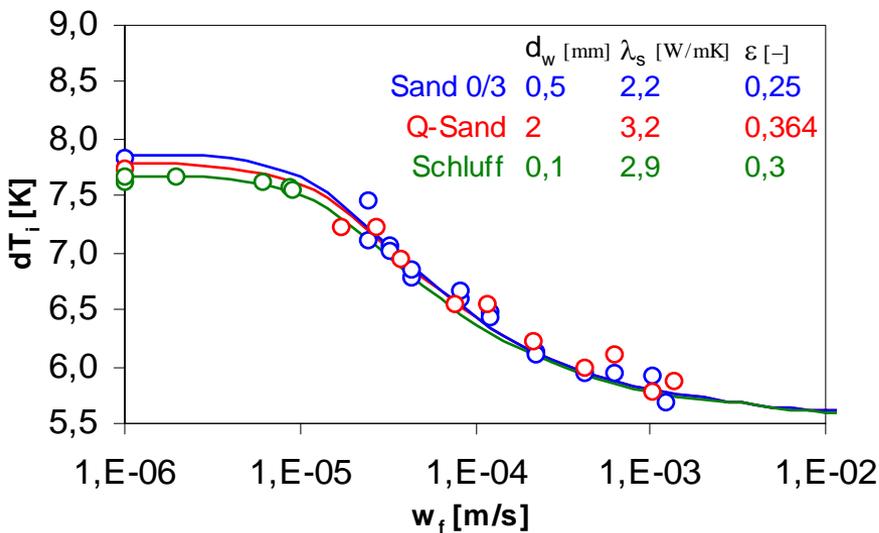


Leakage  
detection : 4  
& 1 l/min?

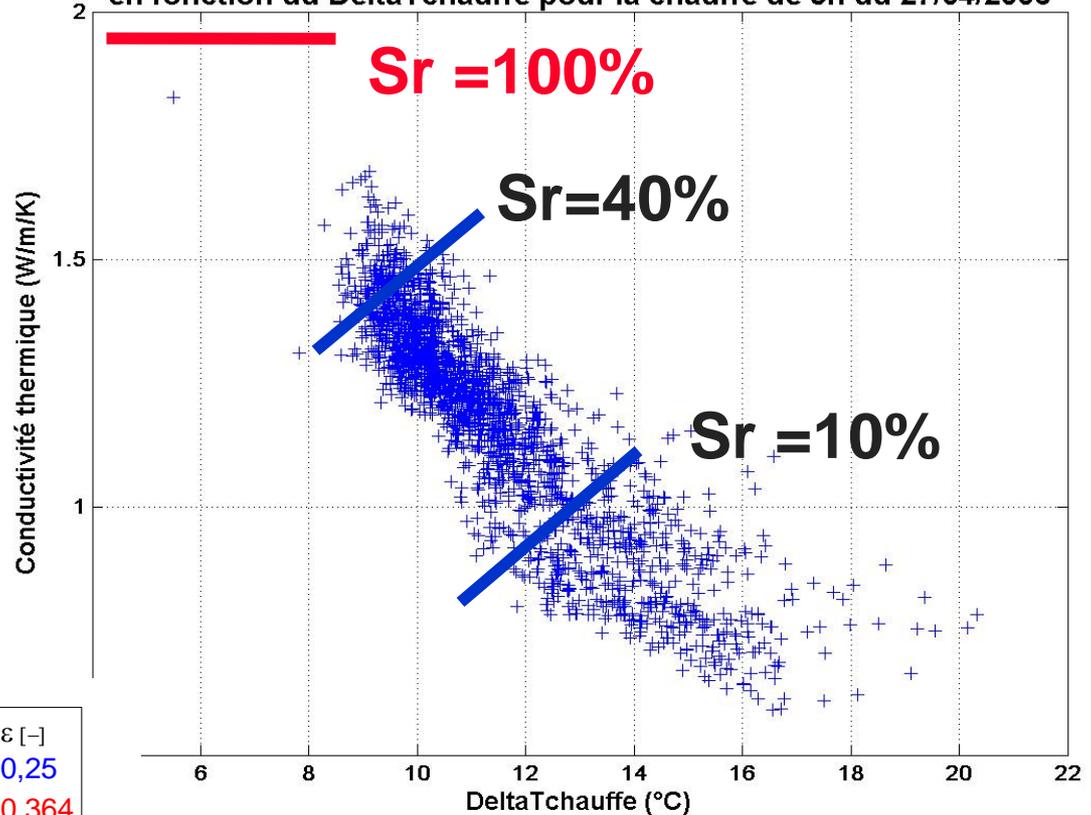
# Preventive maintenance



# Flow velocity (TUM 2006)



Visualisation 1D - Graphique de la conductivité thermique en fonction du DeltaTchauffe pour la chauffe de 5h du 27/04/2006



active method:

No leak at Oraison :  
(EDF 2006)



# Preventive maintenance IJKDIJK Project (NL)

1  
6  
0  
4

## Piping detected by fiber optic in the 4 tests



17:03



16:48



16:33



16:18



16:03



15:48



15:33



15:18



15:03



14:48



14:33



14:18



14:03



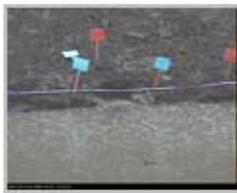
13:48



13:33



13:18



13:03



12:48



12:33



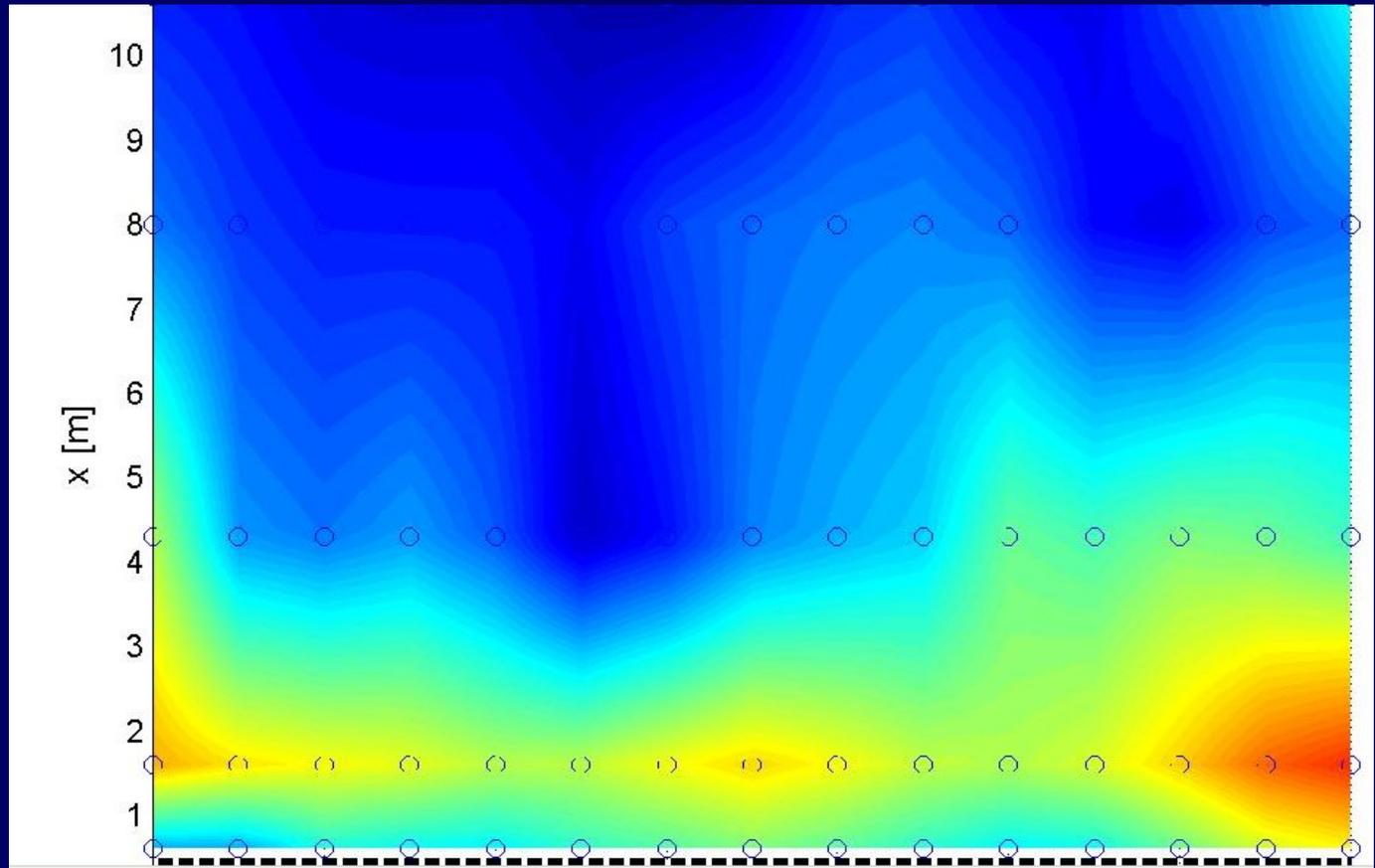
12:18



# IJKDIJK Test 2

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

Detection  
by  
température  
19 october  
2009  
14h58  
24H after  
the start

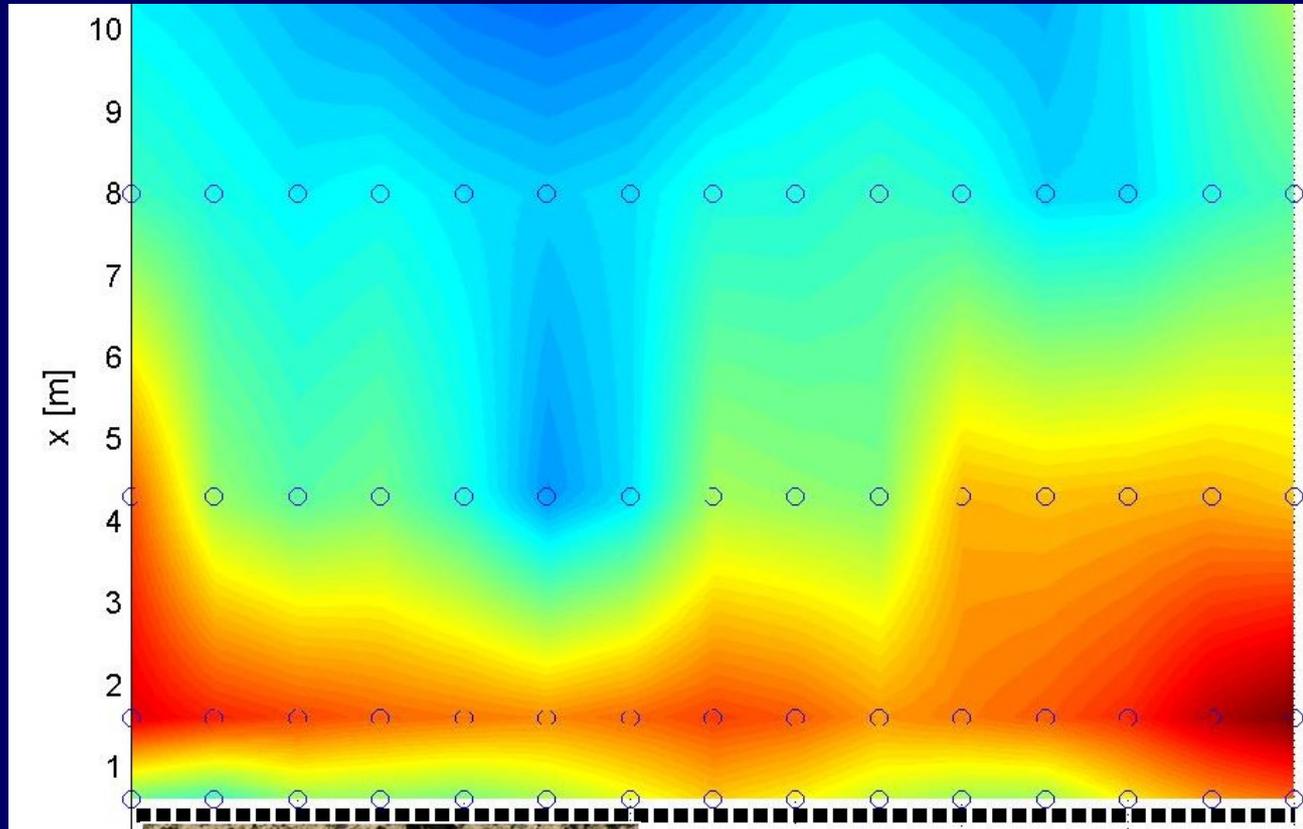




# IJKDIJK Test 2

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

Detection  
by  
température  
20 october  
2009  
11h58

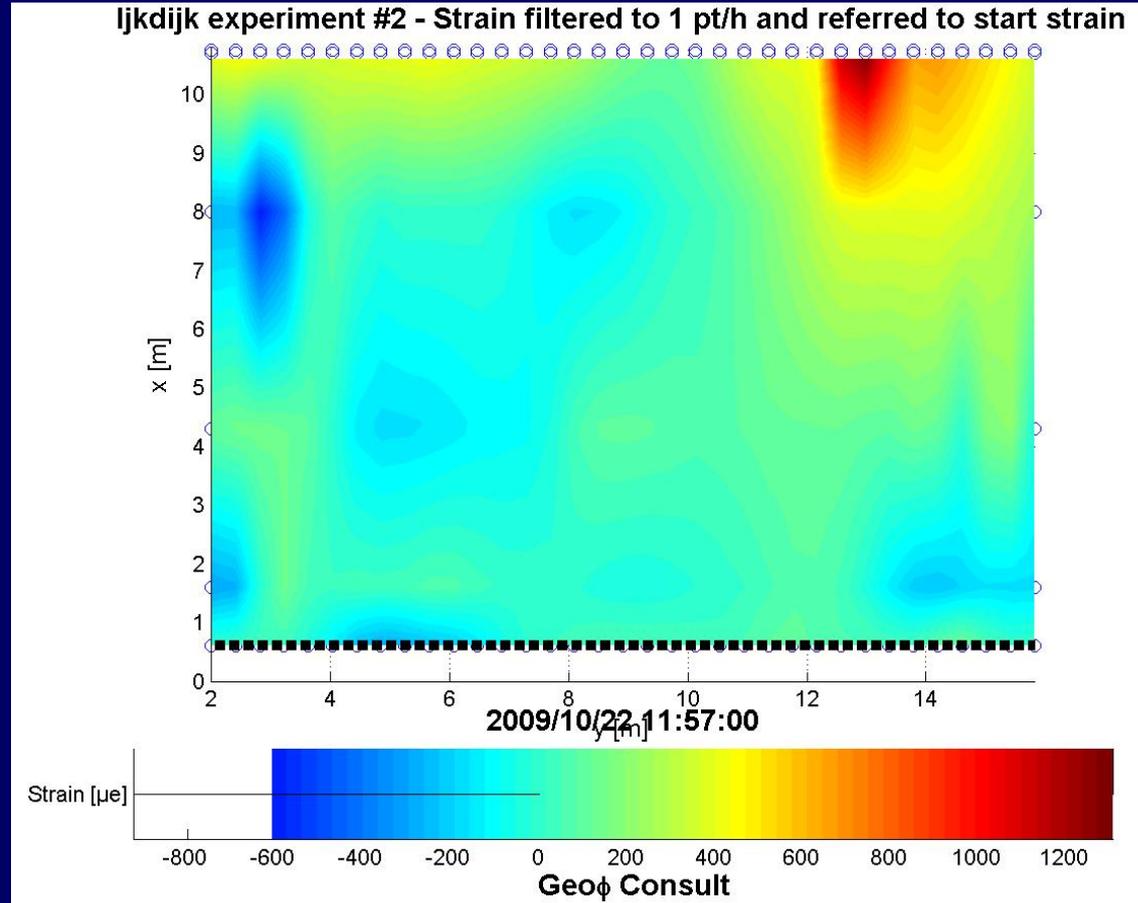




# IJKDIJK Test 2

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

Erosion  
Détection  
with strain  
measurements  
22 October  
2009  
11h57





# References and acknowledgments

1  
6  
0  
4  
2  
0  
1  
0  
M  
A  
D  
R  
I  
D  
C  
N  
E  
G  
P

Assessment of the Risk of Internal Erosion of Water Retaining Structures: Dams, Dykes and Levees

Intermediate Report of the European Working Group of ICOLD

Contributions to the Symposium on 17–19 September 2007 in Freising, Germany

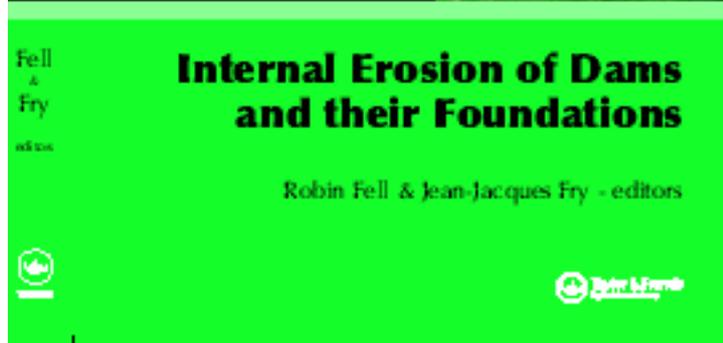


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